# DESIGN AND SCHEDULING OF A MAJOR BUILDING 

## PROJECT

A
THESIS
Submitted in partial fulfillment of the requirements for the award of the degree of

MASTER OF TECHNOLOGY
IN
CIVIL ENGINEERING
With specialization in
CONSTRUCTION MANAGEMENT
Under the supervision
of
Dr. Ashok Kumar Gupta
Professor and Head of Department by

Anil Kumar
(172607)


JAYPEE UNIVERSITY OF INFORMATION TECHNOLOGY
WAKNAGHAT, SOLAN - 173234
HIMACHAL PRADESH, INDIA
MAY - 2019

## STUDENT'S DECLARATION

I hereby declare that the work presented in the Project report entitled "Design and Scheduling of a Major Building Project" submitted for partial fulfillment of the requirements for the degree of Master of Technology in Civil Engineering at Jaypee University of Information Technology, Waknaghat is an authentic record of my work carried out under the supervision of Dr. Ashok Kumar Gupta. This work has not been submitted elsewhere for the reward of any other degree/diploma. I am fully responsible for the contents of my project report.

Signature of Student
Anil Kumar
172607
Department of Civil Engineering
Jaypee University of Information Technology,
Waknaghat, India
Date:

## CERTIFICATE

This is to certify that the work which is being presented in the project report titled "Design and Scheduling of a Major Building Project" in partial fulfillment of the requirements for the award of the degree of Master of Technology in Civil Engineering submitted to the Department of Civil Engineering, Jaypee University of Information Technology, Waknaghat is an authentic record of work carried out by Anil Kumar (172607) during a period from August, 2018 to May, 2019 under the supervision of Dr. Ashok Kumar Gupta, Department of Civil Engineering, Jaypee University of Information Technology, Waknaghat. The above statement made is correct to the best of my knowledge.

Date: $\qquad$

| Signature of Supervisor | Signature of HOD | Signature of External <br> Examiner |
| :--- | :--- | :--- |
| Dr. Ashok Kumar Gupta | Dr. Ashok Kumar Gupta | External Examiner |
| Professor and Head of | Professor and Head of <br> Department | Department |
| Department of Civil <br> Engineering | Engineering |  |
| JUIT, Waknaghat | JUIT, Waknaghat |  |

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## Anil Kumar <br> 172607


#### Abstract

The key objective of this research is to analyze and design a multistoried building project complex using STAAD Pro and then schedule the prime and necessary activities involved in the construction of the building complex with the help of Microsoft Project 2013 and then in the end using Autodesk Revit 2013 we are going to make 3d model of the buildings and take material takeoff for estimate of construction cost .The plan of building complex consists of 4 residential apartments of Six storey building. The design involves load calculations and generating load combinations and analysis of the structure with the help of STAAD Pro. IS: 456(2000) confirms all the design methods used in STAAD-Pro. Different work associated with the project are estimated and the activities are scheduled. Planned cost, time, and materials of the project are acquired by resource allocation. Various activities involved in the construction of this residential building project are estimated and the activities are scheduled, as project starts. Budgeted cost, time, and materials of the project are obtained by resource allocation.


Keywords: STAAD PRO, MSP 2013, Analysis, Design, Revit, Estimation.

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## CHAPTER 1 <br> INTRODUCTION

### 1.1 Outline of the Chapter

We humans from the beginning of era required buildings or structures for live in and to acquire that we want from time to time. But then again it's not only buildings but also to build structure efficiently so that it can fulfill its main purpose. So here comes the role of civil engineering and the role of design and analysis of structure.

This project is of analysis, design, scheduling and estimating construction cost of multistoried building project using a very popular designing software STAAD Pro, Microsoft Project 2013, Revit 2013. We are using STAAD Pro because of its listed below benefits:

1. Simple to utilize interface.
2. Verification with the IS codes.
3. Solving errors in a versatile manner.
4. Planning Precision.

STAAD Pro shows a modern UI, powerful analysis and design engines and picturing tools with advanced finite element and dynamic analysis capabilities. STAAD Pro is every professional's option for concrete design, steel design and cold-formed steel design of low and high-rise buildings for model generation, analysis and design and result verification.

Similarly Microsoft Project 2013 is chosen because of the following advantages:

1. It empowers the undertaking the executive's experts to deal with task portfolio speculations dependent on need, start ventures at the most punctual, and create result inside pre-decided spending plan.
2. Microsoft Project 2013 conveys precise outcomes and furthermore gets ready for the future to deal with monstrous and deficiencies over a skyline.
3. Microsoft Project 2013 conveys extends on time and pursues plan the board adequately. It additionally conveys a system to track the advancement of the undertaking.

Also and for designing the 3 d project Revit software is chosen because of its following advantages:

1. Intelligent 3D-model-based design tools
2. BIM programming for designers, contractors, engineers and architects
3. Create an integrated model that contains genuine data
4. Great for demonstrating, clash recognition and change the management
5. Contains all important structure components just as maker, model, cost, and structure and phase data, among others.

### 1.2 Steps involved in Structural Design

1 Structural design.
2 Calculation of load.
3 Analysis Technique.
4 Member design and Detailing.

### 1.3 Loads Considered

### 1.3.1 Imposed Loads

1 Floor Load $=4 \mathrm{Kn} / \mathrm{m}^{2}$
2 Roof Live Load $=2 \mathrm{Kn} / \mathrm{m}^{2}$

### 1.3.2 Dead Loads

1 Self-Weight of Slab $=0.15 * 25=3.75 \mathrm{Kn} / \mathrm{m}^{2}$
2 DL due to External Wall $=0.35 * 2.45 * 20=19.15 \mathrm{Kn} / \mathrm{m}^{2}$
3 DL due to Partition Wall $=0.2 * 2.5 * 20=11.8 \mathrm{Kn} / \mathrm{m}^{2}$
4 DL due to Parapet Wall $=0.2 * 1.5 * 20=8 \mathrm{Kn} / \mathrm{m}^{2}$
5 Plaster for two face $=0.02 * 2.45 * 1 * 18 * 2=2 \mathrm{Kn} / \mathrm{m}^{2}$

### 1.3.3 Wind Load

Design Wind Speed, $\mathrm{V}_{\mathrm{Z}}$
The design wind speed, $\mathrm{V}_{\mathrm{z}}$ for any place is obtained from:
1 Terrain Roughness, height and size of structure.
2 Local Topography.
3 Risk Level.
Mathematically

$$
\begin{equation*}
\mathrm{V}_{\mathrm{z}}=\mathrm{V}_{\mathrm{b}} * \mathrm{~K}_{1} * \mathrm{~K}_{2} * \mathrm{~K}_{3} \tag{eq. 1}
\end{equation*}
$$

Where:
$\mathrm{V}_{\mathrm{b}}=$ Basic wind speed at any height in $\mathrm{m} / \mathrm{s}$;
$\mathrm{K}_{1}=$ probability factor (risk coefficient)
$\mathrm{K}_{2}=$ terrain, height and structure size factor
$\mathrm{K}_{3}=$ topography factor

### 1.3.4 Seismic Load

Method for Analysis -

1. Equivalent Static Method
2. Lumped Mass Model Method
3. Response Spectrum Method

In this report equivalent static method is used.
Code Used = IS 1893 (Part I), 2002
Total design seismic base shear, $\mathrm{V}_{\mathrm{b}}$ at any main direction is determined from the given below expression:

$$
\mathrm{V}_{\mathrm{b}}=\mathrm{Ah} * \mathrm{~W} \quad \text { eq. } 2
$$

Where,

$$
\begin{align*}
& \mathrm{V}_{\mathrm{b}}=\text { Total Seismic design base shear } \\
& \mathrm{W}=\text { seismic weight of all the floors }(\mathrm{W}=\mathrm{DL}+50 \% \mathrm{LL}) \\
& \mathrm{Ah}=\text { horizontal acceleration spectrum } \\
& \mathrm{Ah}=\frac{Z}{2} * \frac{I}{R} * \frac{S a}{g} \tag{eq. 3}
\end{align*}
$$

Where,

$$
\begin{aligned}
& \mathrm{I}=\text { Importance Factor } \\
& \mathrm{Z}=\text { Zone Factor } \\
& \mathrm{R}=\text { Response Reduction Factor } \\
& \frac{S a}{g}=\text { Design Acceleration Spectrum }
\end{aligned}
$$

### 1.3.5 Loads Combination

For Beams and columns

1. $1.5(\mathrm{DL}+\mathrm{LL})$
2. 1.2(DL+LL+EQX)
3. 1.2(DL+LL-EQX)
4. 1.2(DL+LL+EQZ)
5. 1.2(DL+LL-EQZ)
6. $1.5(\mathrm{DL}+\mathrm{EQX})$
7. 1.5(DL-EQX)
8. 1.5(DL+EQZ)
9. 1.5(DL-EQZ)

For Foundation

1. $\mathrm{DL}+\mathrm{LL}$
2. DL+0.5LL+EQX
3. DL+0.5LL-EQX
4. DL+0.5LL+EQZ
5. DL+0.5LL-EQZ

## CHAPTER 2

## LITERATURE REVIEW

### 2.1 GENERAL

In this thesis main goal is to schedule a project from its beginning till its completion, then analyze the structure for seismic, wind loading and load combinations and after that estimation of cost incurred in the project. So this literature study so far consists of all such research papers that include design of structures, analysis or scheduling of projects.

### 2.2 LITERATURE STUDY

Wale et al [1] Project Managing is information using efficiently, aptitudes and methods to spread maneuvers to see job requirements. It's a vital ability to achieve something efficiently for affiliations, engaging them to fix the project results to Organizational goals. It is often characterized as process \& movement of arranging out, sorting, moving, and monitoring assets, frameworks to accomplish explicit objectives in sound or everyday concerns. A project is an impermanent point projected to create an exceptional thing, organization or result with a described beginning \& finish, embraced to meet unconventional goals. In usage, the organization of these two structures is routinely truly indisputable, and everything considered requires the improvement of extraordinary particular aptitudes and the board strategies.

Kumar K et al [2] Nations around the globe give significant inclination to the development business, as it contribute inconceivably to the development of a country, however utilization of conventional practices and ill-advised arranging diminishes the effectiveness of the development business which influences the venture as expanded span of the undertaking, this prompts the expanded overhead expense of the task and low quality of work. With the end goal to dispose of these imperfections in development venture, a powerful undertaking administration device is presented as Microsoft Project 2013 programming. In this investigation venture planning, estimation and asset designation are adjusted in MK Apartment private development venture utilizing MSP 2013 programming. Different work associated with the development of MK condo venture are evaluated and the exercises are planned, as undertaking beginning structure first Aug 2016 and completing on 29th July 2017. Planned cost, time, and materials of the venture are acquired by asset portion.

Nalwadgi et al [3] presently multi day expansive number of utilization programming's are accessible in the structural building field. All these products are created as the premise of cutting edge. Limited component examination which incorporate the impact of dynamic load, for example, wind impact, earth tremor impact wagers and also in the today's work, an endeavor has been made to consider the adequacy of certain basic planning application
programming hence an on-going task has been picked. This undertaking has a spot with the solidarity producers to be executed in the Gulbarga City. Bharat pride is the name of the undertaking.

Rani.H and Babu [4] their work included the study and planning of multistory (G+4) building with the help of STAAD Pro. They used STAAD Pro coz of its favorable features like easy to use interface, IS code confirmation, adaptable nature of solving problems, the precision of arrangement. Staad Pro is everyone's choice for design of concrete, steel, timber, aluminum and cold shaped steel structure of low \& elevated structure. In their work, a G+4 storey private building is broke down using E-Tabs and traditional building material are replaced by green material making the building eco-friendly, energy efficient and economical.

Hussian et al [5] their work was to plan a multi-storied working of G+ 5 stories, at kalakode around 4 km from paravoor. The plan is finished by considering the necessities and principles suggested by IS code, Kerala building standards and national building rules. Arranging is finished utilizing the 3D demonstrating programming Revit 2011 with the assistance of Auto CAD 2014. The structure examination and configuration is finished utilizing STAAD.PRO.V8i and a cross-check is improved the situation chosen individuals utilizing limit state technique for plan according to IS 456-2000. STAAD. Professional uses a direction dialect based info arrange, which can be made through an editorial manager called the supervisor document, the incredible STAAD.Pro illustrations input generator or through CAD based information generators like AutoCAD. The yield produced by staad.pro comprises of point by point numerical outcomes for examination what's more, design.

Sharma \& Maru [6] Investigation and plan of structures for static powers is a standard issue nowadays due to the approachability of reasonable specific projects which can be utilized for the investigation. Then again, the dynamic investigation is a tiresome procedure and needs spare info identified with the form of the structure, and a conception of basic elements for the elucidation of diagnostic consequences. Strengthened cement structures are the most wellknown sort of development in city areas, which are exposed to a few kinds of influences amid their period of lifespan, for example, static powers because of DL \& LL and dynamic powers because of the breeze and tremor. Here the present works (the issue has taken) are on a G+30 storied normal building. These structures have the arrangement region of $30 \mathrm{~m} \times 45 \mathrm{~m}$ with a story tallness 3.8 m each and profundity of the establishment is 3.0 m . and add to the stature of a picked building together with profundity of the establishment as 120 m .

Shivashaankar \& Yashwant [7] the paper presents the various limitations in design and construction practices along with the feedback to overcome the limitations and make the structures safer to take the earthquake forces. The paper focuses on software used in the civil engineering for analysis and design, construction methods/practices, use of materials, types of structures, experiments for earthquake studies, quality control parameters etc.

Sharma, Abhishek \& Pathak, K. K. [8] Improper planning, scheduling and execution works that results in several issues like reduction in quality of construction, delay in providing facilities, development, and making the project more expensive. A report suggested that the supply of manpower is inversely proportional to time required to complete the project. As the manpower is increased, the completion time of the project is decreased and vice versa. Present study deals with the manpower planning, scheduling and tracking of "Construction of a Residential Block at Shakti Kunj, Ahmedabad", a six storied (G+6) building project whose construction is in progress at Shakti Kunj, Ahmedabad, Gujarat. An evaluation between the baseline duration and cost to actual duration and cost of manpower of project is also determined using MSP 2013.

Paulay, T. and Priestley, M.N. [9] underscores genuine structure design, not analysis of multistory structures for seismic obstruction. Solid prominence is set on explicit specifying necessities for development. Key plan standards are introduced to make structures that react to a wide scope of potential seismic powers, which are outlined by various nitty gritty models. The discourse incorporates the plan of strengthened cement flexible casings, auxiliary dividers, double frameworks, and fortified stone work structures, structures with confined malleability and establishment dividers. Notwithstanding the precedents, full plan figuring's are given for three model structures.

Clough Ray W. and King Ian P. [10] an effective advanced PC strategy for the auxiliary investigation of huge, multistory building outlines is displayed. The structure might be exposed to both vertical and sidelong loadings and may incorporate a subjective arrangement of shear dividers. Hub and shear contortions, and in addition flexural twists of the individuals, might be considered. The strategy depends on the improvement of a tri-corner to corner firmness network of each casing in the building, its decrease by recursion connections to the parallel casing solidness, lastly the super stiffness of the total building. Results acquired for a precedent structure are assessed.

Chopra Anil K. and Gutierrez Jorge A. [11] in view of the Ritz idea, for dynamic investigation of the reaction of multistorey structures including establishment communication to seismic tremor ground movement, is displayed. The framework considered is a shear expanding on an unbending round circle balance joined to the surface of a directly versatile halfspace. In this strategy, the basic relocations are changed to ordinary methods of vibration of the expanding on an inflexible establishment. The investigation method is created and numerical outcomes are exhibited to show that phenomenal outcomes can be acquired by considering just the initial couple of methods of vibration. As the quantity of questions is diminished by changing to summed up directions, the technique introduced is substantially more proficient than direct strategies.

Choi, C., Chung, H., Lee, D., \& Wilson, E. L. 12] the impact of the consecutive utilization of dead load due to the successive nature of development is an essential factor to be considered
in the multistory edge examination. Shockingly, nonetheless, this impact has been disregarded by numerous designers practically speaking previously. One of the approaches to incorporate this impact legitimately in the examination is to bring out the investigation through wellordered techniques as per the successful utilization of dead loads as the development continues. These systems, nonetheless, require explained calculations and more arrangement time. A streamlined methodology, named as adjustment factor strategy (CFM), to take care of the issue without explained well-ordered examinations has been proposed in this paper. This strategy uses the rectification factors built up by a relapse from the information got from the current structures to change the outcomes from the standard investigation to deliver more precise arrangements. Some numerical tests are exhibited to demonstrate the legitimacy and adequacy of the technique.

Abishek and Pathak [13] Investigated the connection between the task finish time and the labor accessibility as contrarily relative that is the fruition time of the undertaking can be diminished, by expanding the labor. For the present investigation, the creator considered a multi-story building development named "Mahadev Parisar at Shivaji nagar Bhopal". The venture characteristics comprises of $\mathrm{G}+6$ floors private condos with 92 pads in it. With an accessible land territory of 2.64 sections of land at Shivajinagar Bhopal with, he evaluated the length of culmination of two years, however the task was postponed. In this venture, MSP2013 is utilized as the task the board device, and two-stage system is received in this undertaking planning process. In the principal stage, the data accessible from the site and every one of the illustrations accessible are gathered, the amounts of materials going into the venture are evaluated and arranged. For the second stage, different exercises engaged with the development of the flat are recorded in the MSP 2013, these exercises are separated utilizing WBS application in MSP into subtasks. The movement begin and complete dates are characterized physically or utilizing auto plan choice, different assets accessible for the development of the venture are distributed and the basic way of the task is given by MSP2013, the gauge of the undertaking was set and the exercises are followed for finishing the fragmented exercises were rescheduled accordingly the evaluated time of fulfillment was surpassed from 693 days to 1424 days, the expense of labor was surpassed from 2.5 crores to 3.1 crores . The fluctuation cost of 67 lakhs and the difference time of 731 days were found because of the utilization of planning.

Rhuta and Patil [14] examine the development venture the board in different nations like USA, Canada, and Australia. Looks at the development venture arranging situation over the development venture at ground execution organize, where a portion of the thing that matters is seen as in the event of the arranging procedure, it is accepted that everything runs easily, it isn't the equivalent if there should be an occurrence of genuine undertaking situation, accessibility of assets might be restricted Resolving this utilizing a task the board programming MSP 2013. This is settled by leveling the assets and contrasting the time cost usage and a booked time and assessed cost. Venture the board strategies like CPM/PERT are adjusted with
the end goal to determine different deformities, for example, over allotment, lopsided utilization of assets and to anticipate the cutting edge issues emerging in the undertaking. for this situation ponder, the two-stage strategy was received in the main stage different undertaking related information are gathered from the site, the amount of work that should be performed was determined and the computations were arranged, in the second stage all the task related exercises are recorded consecutively utilizing MSP2013.

Suresh and Nanduri [15] the sentiment that structuring quake resistant structures will cause considerable further costs. In a Swiss outline assesses some place in the scope of 3 and $17 \%$ of the hard and fast structure and their costs are specified. The investigation method is created and numerical outcomes are exhibited to show that phenomenal outcomes can be acquired by considering just the initial couple of methods of vibration. As the quantity of questions is diminished by changing to summed up directions, the technique introduced is substantially more proficient than direct strategies.

Behera and Debeshish [16] in todays advanced time the structures are made to fulfill our fundamental points of view. It's definitely not a problem to build up a Structure regardless it is basic to fabricate a viable structure which will serve for quite a while without showing any mistake. This study focuses in searching good strategy for making geomtry, defining the cross zones of segment \& shaft. Creating assurance and supports (to describe an assistance atmosphere it is fixed or pinned) \& after it the loads are portrayed. Then the model is explored by run analysis, after it keep an eye on the loading screen and look for errors \& warnings and if not any ,then the structure is safe for design.

Adiyanto and Zaini [17] the impact of the consecutive utilization of dead load due to the successive nature of development is an essential factor to be considered in the multistory edge examination. Shockingly, nonetheless, this impact has been disregarded by numerous designers practically speaking previously. One of the approaches to incorporate this impact legitimately in the examination is to bring out the investigation through well-ordered techniques as per the successful utilization of dead loads as the development continues. These systems, nonetheless, require explained calculations and more arrangement time. A streamlined methodology, named as adjustment factor strategy (CFM), to take care of the issue without explained well-ordered examinations has been proposed in this paper. This strategy uses the rectification factors built up by a relapse from the information got from the current structures to change the outcomes from the standard investigation to deliver more precise arrangements. Some numerical tests are exhibited to demonstrate the legitimacy and adequacy of the technique.

Thakur and Singh [18] Shear divider frameworks are a standout amongst the most ordinarily utilized parallel burden opposing framework in tall structures, Shear divider has extremely high in plane solidness and quality which could be utilized to all the while oppose expansive even loads and bolster vertical or gravity loads making them very worthwhile in numerous
basic designing applications. In multistory structure to oppose parallel powers joining of Shear dividers has turned out to be inescapable. It is important to decide successful, effective and perfect area of shear divider. This analysis of G+4 Story (Zone IV) is specified some primer consideration that is dissected through change in different position of shear divider with various shapes to decide factor i.e. storey drift \& minutes. Thus investigation is finished by operating Software pack STAAD Pro.

Ambadkar and Bawner [19] studied the effects of wind on structures. Wind loads as specified in IS: 875 (Part 3) - 1987 were considered in the analysis. In this project analysis of $G+11$ building. Analysis is done for various variations such as 1) Terrain with few or no obstructions having heights below 1.5 m . 2) Terrain with obstructions having heights between 2.0 to 10 m . 3) Terrain with many close spaced obstacles having the size of building structures up to 10 m high. 4) Terrain with many hefty high close spaced obstacles. Conferring to Internal Pressure Coefficients (Cpi) providing for that many variations. This analysis is done for wind speed 45 $\mathrm{m} / \mathrm{s}, 48 \mathrm{~m} / \mathrm{s}, 52 \mathrm{~m} / \mathrm{s}$. Results gotten from STAAD-PRO analysis are used for finding major associations of moments, forces and displacement with wind speeds. Moments, forces and displacement obtained from all cases are related with wind speeds, conferring to their percentage of opening if for many variations.

Arya and Khan [20] in this examination paper, the impact of wind speed and auxiliary reaction of structure outline on slanting ground has been contemplated. Thinking about different casing geometries and incline of grounds. Blend of static and wind loads are considered. For blend, 60 cases in various breeze zones and three distinct statures of structure outlines are broke down. STAAD-Pro v8i programming has been utilized for investigation reason. Results are gathered as far as pivotal power, Shear power, minute, bolster response, Story-wise float and Displacement which are fundamentally examined to evaluate the impacts of different slant of ground.

### 2.2 OBJECTIVE OF STUDY

The fundamental target of this examination is:

1. Analysis and Design of different basic parts of the modular building.
2. To schedule various activities included in the overall construction of a building
3. To evaluate the cost required to finish the task with effectiveness.

## CHAPTER 3

## Methodology

### 3.1 Outline of Chapter

The fundamental step in the methodology includes designing, scheduling and cost optimization of the project. Designing phase includes Six storey building design in Staad pro which further includes loads calculations and concrete design. Then the scheduling phase is carried out by using Microsoft Project 2013, in which all the important activities occurring in a construction project are listed and a calendar is created specifying start date, finish date and exceptions etc. And lastly after all the resources and activities are allocated and scheduled respectively, cost of the materials, labor, and construction are calculated.


### 3.2 MODELLING:

### 3.2.1 Structure Generation

Plan of the building is designed in STAAD and after applying translational repeat no. of floor is given and frame model is generated. Fig. 3.2.1.1 shows the 3d frame model of structure.
$Y_{z}^{x}$


Fig 3.2.1.1 3d view of frame model

### 3.2.2 Assigning Properties

1. Size of Beam $-0.3^{*} 0.3 \mathrm{~m}$
2. Size of Column $-0.6 * 0.6 \mathrm{~m}$
3. Slab Thickness -150 mm
4. Height of each Floor $-3 m$
5. Material-Concrete
6. Support - Fixed

As above mentioned specifications property for beams and columns and thickness of plate are defined and assigned. Supports are assigned as shown in Fig. 3.2.2.1 \& Fig. 3.2.2.2 shows beams, columns and slabs assigned to the project.


Fig. 3.2.2.1 showing columns beams and supports


Fig.3.2.2.2 3D picture showing beams, columns and plates

### 3.2.3 Load and Definitions

Before assigning any loads to the structure firstly we need to define seismic and wind definitions for seismic and wind load to act on the structure. For specifying the wind definition Go to wind definitions and click Add after it is added, add Intensity and exposure manually as per IS 875 Part-3 Intensity provided is given in Table 3.2.3.1, After this definition is added. Go to seismic definition, Click add, Select Code, after clicking on (IS 1893-2002) fill the zone factor importance factor structure type etc. as per code. Applied loads definitions and combinations as per Fig. 3.2.3.1, Fig. 3.2.3.2, Fig. 3.2.3.3.

Table 3.2.3.1 Wind load intensity at different heights

| S.No. | Height <br> $(\mathrm{m})$ | Intensity |
| :---: | :---: | :---: |
| 1 | 3 | 0.75 |
| 2 | 6 | 0.9 |
| 3 | 9 | 0.99 |
| 4 | 12 | 1.10 |
| 5 | 15 | 1.25 |
| 6 | 18 | 1.37 |



Fig.3.2.3.1 Dialog box showing Load cases details \& Load Definitions


Fig. 3.2.3.2 Showing Dead load \& Live Load acting on structure


Fig.3.2.3.3 showing seismic load acting in X direction with displacement

### 3.2.4 Concrete Design

After creating and assigning loads definitions and combinations, design for concrete is started. It is done as per IS 456 (2000) with the help of code important parameters are defined like CLEAR, FC, FYMAIN, MAXMAIN. After filling these parameters commands for designing beam, column, slab, and for takeoff is given and after that all these are assigned to the project.


Fig. 3.2.4.1 Dialog box showing concrete design

### 3.2.5 Design Analysis/Print

In the last step analysis/print command is given and assigned and then analysis is run for possible errors or warnings as shown in Fig. 3.2.5.1


Fig. 3.2.5.1 Dialog box showing analysis print and result

### 3.2.6 Interactive Concrete design

After analysis is done, we go for concrete design mode in Staad Pro for design of beam, column and slabs. For this open concrete design tab, and once window is open.

1. Create Envelope and name it as it suits us.
2. After this select the load cases you would like to design the project for, Fig. 3.2.6.1 shows window of envelope.


Fig.3.2.6.1 Envelope window in concrete design
3. After envelope is created, select the beams and columns and form members.
4. Then members are created, go to Groups/Briefs and add new briefs for beams, columns and slab as shown in Fig. 3.2.6.2 (a) (b) (c).


Fig. 3.2.6.2 (a) Design brief for beam


Fig. 3.2.6.2 (c) Design Brief for slabs
4. After designing briefs add the members into design groups and slabs into slab design group.


Showing beams and columns as members

5. Then after designing groups and briefs, go to concrete member tab and start designing beam, columns and slab as shown in Fig. 3.2.6.3 (a), (b), (c).


Fig. 3.2.6.3(a) Beam design window


Fig. 3.2.6.3(b) Column design window


Fig. 3.2.6.3(c) Slab design window
6. Beams, column and slab design is done then foundation design is started. For it go to foundation design wizard and include the load cases for foundation design and run STAAD Foundation as shown in Fig. 3.2.6.4


Fig. 3.2.6.4 Showing Foundation design window
7. Once STAAD Foundation opens, create Job for isolated foundation and set parameters as shown in Fig 3.2.6.5(a) (b) (c) (d) (e).


Fig. 3.2.6.5(a) Job setup window


Fig. 3.2.6.5(b) Concrete \&rebar input window

Fig. 3.2.6.5(c) Cover \& soil input window
Sliding and Overturning

| Coefficient of friction | 0.5 |
| :--- | :--- |
| Factor of safety against <br> sliding | 1.5 |
| Factor of safety against <br> overturning | 1.5 |



Fig.3.2.6.5 (d) Sliding \& overturning window


Fig. 3.2.6.5(e) Footing Geometry window
8. After setting and defining all the parameters for foundation design, run the design and analyze.

### 3.3 SCHEDULING

Create and schedule a new project

1. Open MSP 2013 software.
2. First of all before starting listing activities, we need to specify the calendar for the project.
3. For that click on "Project" option and then select "Change Working Time" and design the calendar as per your desire like here as shown in Fig. 3.3.1.
4. And after that start listing all the activities with start date or finish date and MSP will schedule it automatically or manually.

Preparing calendar for project with exceptions and holidays till start and finish date

Exceptions Work Weeks

| Name | Start | Finish | $\wedge$ |
| :---: | :---: | :---: | :---: |
| Republic Day | 1/26/2019 | 1/26/2019 |  |
| Maha Shivaratri | 2/4/2019 | 2/4/2019 |  |
| Holi | 3/20/2019 | 3/20/2019 |  |
| Ramzan | 6/5/2019 | 6/5/2019 |  |
| Bakr Id | 8/12/2019 | 8/12/2019 |  |
| Independence Day | 8/15/2019 | 8/15/2019 |  |
| Ganesh Chaturthi | 9/2/2019 | 9/2/2019 |  |
| Muharam | 9/10/2019 | 9/10/2019 |  |
| Gandhi Jayanti | 10/2/2019 | 10/2/2019 |  |
| nureahrs | 10/8/3n10 | 10/8/7n10 | $\checkmark$ |

Fig.3.3.1 Dialog box showing project calendar

In the project calendar, working hours are set to 8 hours with 1 hour break for rest and lunch for laborers and employees etc.

After calendar is set, start listing all the activities and duration and specify schedule auto/manual based on your convenience, here it is set on auto schedule means it will adjust duration and start and finish dates itself. Below fig.3.3.2 shows activities listed

| WBS - | Task <br> Mode | Task Name - | Duration - | Start | Finish | Predecessors |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $\lambda$ | $\triangle$ Start | 516,4 days | Tue 1/1/19 | Thu 1/7/21 |  |
| 1.1 | * | Prepare Contract Drawings | 38 days | Tue 1/1/19 | Mon 2/25/19 |  |
| 1.2 | $\square$ | $\triangle$ Project Procurment | 524,3 days | Tue 1/1/19 | Tue 1/19/21 |  |
| 1.2.1 | $\pm$ | Subcontractor Bid \& Interview Period | 15 days | Tue 1/1/19 | Mon 1/21/19 |  |
| 1.2.2 | $\lambda$ | Recommendatiı \& Approval of Subcontractors | 15 days | Tue 3/26/19 | Mon 4/15/19 | 2 |
| 1.2.3 | $\lambda$ | Other Material Procurment | 191 days | Tue 2/26/19 | Mon 12/2/19 | 2 |
| 1.2.4 | $\square$ | - Construction | 475,3 days | Wed 3/13/19 | Tue 1/19/21 |  |
| 1.2.4.1 | $\lambda$ | Foundation | 70 days | Wed 3/13/19 | Thu 6/20/19 |  |
| 1.2.4.2 | $\lambda$ | Concrete Columns (1st Floor) | 15 days | Wed 3/13/19 | Wed 4/3/19 |  |

Fig.3.3.2 WBS in MSP 2013

After this relations are decided for activities. Generally there are 4 types of relations in MSP 2013.

1. Start to Finish
2. Start to-Start
3. Finish to-Finish.
4. Finish to Start

As shown above in Fig.3.3.2 activities listed are assigned relations based on predecessors and successors. After assigning relations critical path is shown in the Fig.3.3.3 below



Fig.3.3.3 Networking of the Activities by Critical Path Method

And adding all the activities in the MSP 2013 Activities are scheduled and project duration is calculated. Also resources used can be easily monitored and handled with it.

## CHAPTER 4

## Results and Discussions

### 4.1 SCHEDULING

Work Burndown - Shows how much work you have completed and how much you have left. If the remaining cumulative work line is steeper, then the project may be late.


From the beginning of the Project the resources are on use and track can be kept on it easily with the help of graphs and bar charts.


In the above bar chart $82 \%$ work shown is completed and only $18 \%$ work is left.
With the help of software after shifting the project start date and scheduling and levelling the resources it is known that the Project ends in 524 days using all the available resources.

### 4.2 Loads Considered

Dead Loads
1 DL due to Plate $/$ Slab $=0.15 * 25=3.75 \mathrm{kN} / \mathrm{m}^{2}$
2 DL due to External Wall $=0.35 * 2.45 * 20=19.15 \mathrm{kN} / \mathrm{m}^{2}$
3 DL due to Partition Wall $=0.2 * 2.5 * 20=11.8 \mathrm{kN} / \mathrm{m}^{2}$
4 DL due to Parapet Wall $=0.2 * 1.5 * 20=8 \mathrm{kN} / \mathrm{m}^{2}$
5 Plaster for two face $=0.02 * 2.45 * 1 * 18 * 2=2 \mathrm{kN} / \mathrm{m}^{2}$
Imposed Loads

1. Roof Live Load $=2 \mathrm{kN} / \mathrm{m}^{2}$
2. Floor Load $=4 \mathrm{kN} / \mathrm{m}^{2}$

Design Load
For the design of the beam, column and slab we've considered load combination L/C \#14 which is $1.2(\mathrm{DL}+\mathrm{LL}-\mathrm{EQZ})$.

### 4.3 Deflected Shape

Below shown figure is the deflected shape of the building under Load combination
$\mathrm{L} / \mathrm{C}=1.2(\mathrm{DL}+L L-E Q Z)$.


Fig. 4.3.1 Deflected shape

### 4.4 Max Displacement at nodes

Table 4.4.1 Max Displacement at different nodes

|  |  |  | Horizontal |  |  | Vertical | Horizontal | Resultant | Rotational |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Node | L/C | X mm | Y mm | Z mm | mm | rX rad | rY rad | rZ rad |  |  |
| Max X | 54 | 141.2 (DL+LL-EQZ) | 0.029 | -0.408 | -4.218 | 4.238 | -0.002 | -0.000 | 0.000 |  |  |
| Min X | 49 | 141.2 (DL+LL-EQZ) | -0.029 | -0.408 | -4.218 | 4.238 | -0.002 | 0.000 | -0.000 |  |  |
| Max Y | 2 | 141.2 (DL+LL-EQZ) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |  |  |
| Min Y | 80 | 141.2 (DL+LL-EQZ) | 0.007 | -2.018 | -29.432 | 29.501 | -0.000 | 0.000 | -0.000 |  |  |
| Max Z | 2 | 141.2 (DL+LL-EQZ) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |  |  |
| Min Z | 248 | 141.2 (DL+LL-EQZ) | 0.004 | -0.880 | -29.458 | 29.471 | -0.001 | -0.000 | -0.000 |  |  |
| Max rX | 2 | 141.2 (DL+LL-EQZ) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |  |  |
| Min rX | 181 | 141.2 (DL+LL-EQZ) | 0.012 | -0.459 | -11.457 | 11.466 | -0.002 | 0.000 | -0.000 |  |  |
| Max rY | 218 | 141.2 (DL+LL-EQZ) | 0.017 | -0.248 | -4.230 | 4.237 | -0.002 | 0.000 | -0.000 |  |  |
| Min rY | 221 | 141.2 (DL+LL-EQZ) | -0.017 | -0.248 | -4.230 | 4.237 | -0.002 | -0.000 | 0.000 |  |  |
| Max rZ | 126 | 141.2 (DL+LL-EQZ) | -0.012 | -1.523 | -29.436 | 29.475 | -0.001 | -0.000 | 0.000 |  |  |
| Min rZ | 121 | 141.2 (DL+LL-EQZ) | 0.012 | -1.523 | -29.436 | 29.475 | -0.001 | 0.000 | -0.000 |  |  |
| Max Rst | 207 | 141.2 (DL+LL-EQZ) | 0.003 | -1.934 | -29.447 | 29.510 | -0.000 | -0.000 | -0.000 |  |  |

From the above table it is shown that what is the displacement at different nodes and it is concluded that max. Displacement at different nodes is less than 30 mm .

### 4.5 Max S.F \& B.M at Different nodes

Table 4.5.1 Max SF \& BM at different nodes

|  | Beam | L/C | Node | Fx kN | Fy kN | Fz kN | Mx kNm | My kNm | Mz kNm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Max Fx | 98 | 141.2 (DL+LL-EQZ) | 44 | 1551.114 | 6.097 | 129.665 | 0.252 | -344.366 | 5.240 |
| Min Fx | 542 | 141.2 (DL+LL-EQZ) | 176 | -11.911 | 71.511 | -0.051 | -0.008 | 0.018 | 74.625 |
| Max Fy | 166 | 141.2 (DL+LL-EQZ) | 88 | 1429.768 | 141.236 | -0.218 | -0.002 | 0.286 | 356.097 |
| Min Fy | 289 | 141.2 (DL+LL-EQZ) | 204 | 1.362 | -52.368 | -0.017 | 0.315 | -0.018 | 37.394 |
| Max Fz | 99 | 141.2 (DL+LL-EQZ) | 45 | 1416.382 | -0.327 | 141.833 | -0.015 | -356.536 | -0.435 |
| Min Fz | 392 | 141.2 (DL+LL-EQZ) | 242 | 104.492 | -11.689 | -15.402 | 0.475 | 43.073 | -15.277 |
| Max Mx | 365 | 141.2 (DL+LL-EQZ) | 215 | 661.520 | 0.790 | 95.251 | 1.013 | -310.489 | -0.116 |
| Min Mx | 362 | 141.2 (DL+LL-EQZ) | 212 | 661.523 | -0.791 | 95.251 | -1.013 | -310.490 | 0.115 |
| Max My | 111 | 141.2 (DL+LL-EQZ) | 63 | 940.678 | -0.274 | 105.025 | 0.008 | 183.101 | 0.408 |
| Min My | 99 | 141.2 (DL+LL-EQZ) | 45 | 1416.382 | -0.327 | 141.833 | -0.015 | -356.536 | -0.435 |
| Max Mz | 166 | 141.2 (DL+LL-EQZ) | 88 | 1429.768 | 141.236 | -0.218 | -0.002 | 0.286 | 356.097 |
| Min Mz | 166 | 141.2 (DL+LL-EQZ) | 94 | 1399.162 | 141.236 | -0.218 | -0.002 | -0.367 | -67.612 |

### 4.6 Column Design

Design Load for which columns are designed $=1.2($ DL+LL-EQZ $)$

Member 105 (Main reinforcement layout)


Member 105 ( Shear Reinforcement layout )


Below here is the table of main reinforcement for all columns.
Table 4.6.1 Main Reinforcement

| Mem | L/C | Axial <br> kN | Major kNm | Minor <br> kNm | Design Axis | As Req. $\mathrm{mm}^{2}$ | Total Bars | $\begin{gathered} \text { As Prov. } \\ \mathrm{mm}^{2} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M73 | C14 | 1078.424 | 351.566 | 613.464 | Biaxl min | 11781 | 24 T 25 | 11781 |
| M74 | C14 | 1168.933 | 381.072 | 650.976 | Biaxl min | 11781 | 24 T25 | 11781 |
| M75 | C14 | 1168.994 | 381.092 | 650.722 | Biaxl min | 11781 | 24 T25 | 11781 |
| M76 | C14 | 664.245 | 216.544 | 488.094 | Biaxl min | 7854 | 16 T 25 | 7854 |
| M77 | C14 | 1081.148 | 352.454 | 616.366 | Biaxl min | 11781 | 24 T 25 | 11781 |
| M78 | C14 | 1551.108 | 505.661 | 763.164 | Biaxl min | 15708 | 32 T 25 | 15708 |
| M79 | C14 | 1417.863 | 462.223 | 737.912 | Biaxl min | 15708 | 32 T 25 | 15708 |
| M80 | C14 | 1417.336 | 462.052 | 737.546 | Biaxl min | 15708 | 32 T 25 | 15708 |
| M81 | C14 | 1344.986 | 438.466 | 711.287 | Biaxl min | 13744 | 28 T 25 | 13744 |
| M82 | C14 | 661.520 | 215.656 | 489.100 | Biaxl min | 7854 | 16 T 25 | 7854 |
| M83 | C14 | 1479.229 | 482.229 | 733.612 | Biaxl min | 15708 | 32 T 25 | 15708 |
| M84 | C14 | 1416.380 | 461.740 | 738.958 | Biaxl min | 15708 | 32 T 25 | 15708 |
| M85 | C14 | 1429.768 | 356.097 | 0.367 | Biaxl maj | 3927 | 8 T 25 | 3927 |
| M86 | C14 | 1204.389 | 286.042 | 435.048 | Biaxl min | 7854 | 16 T 25 | 7854 |
| M87 | C14 | 1430.450 | 466.327 | 742.138 | Biaxl min | 15708 | 32 T 25 | 15708 |
| M88 | C14 | 1418.821 | 462.536 | 738.876 | Biaxl min | 15708 | 32 T 25 | 15708 |
| M89 | C14 | 858.693 | 279.934 | 557.189 | Biaxl min | 9817 | 20 T 25 | 9817 |
| M90 | C14 | 1479.232 | 482.229 | 733.613 | Biaxl min | 15708 | 32 T 25 | 15708 |
| M91 | C14 | 1416.382 | 461.741 | 738.959 | Biaxl min | 15708 | 32 T 25 | 15708 |
| M92 | C14 | 1429.770 | 466.105 | 742.135 | Biaxl min | 15708 | 32 T 25 | 15708 |
| M93 | C14 | 1430.452 | 466.327 | 742.139 | Biaxl min | 15708 | 32 T 25 | 15708 |
| M94 | C14 | 1418.823 | 462.536 | 738.877 | Biaxl min | 15708 | 32 T 25 | 15708 |
| M95 | C14 | 858.695 | 279.935 | 557.190 | Biaxl min | 9817 | 20 T 25 | 9817 |
| M96 | C14 | 1081.150 | 352.455 | 616.367 | Biaxl min | 11781 | 24 T 25 | 11781 |
| M97 | C14 | 1551.114 | 505.663 | 763.166 | Biaxl min | 15708 | 32 T 25 | 15708 |
| M98 | C14 | 1417.868 | 462.225 | 737.914 | Biaxl min | 15708 | 32 T 25 | 15708 |
| M99 | C14 | 1417.342 | 462.053 | 737.548 | Biaxl min | 15708 | 32 T 25 | 15708 |
|  |  |  |  |  |  |  |  |  |
| M100 | C14 | 1344.991 | 438.467 | 711.289 | Biaxl min | 13744 | 28 T 25 | 13744 |
| M101 | C14 | 661.523 | 215.656 | 489.101 | Biaxl min | 7854 | 16 T 25 | 7854 |
| M102 | C14 | 1078.427 | 351.567 | 613.466 | Biaxl min | 11781 | 24 T25 | 11781 |
| M103 | C14 | 1168.936 | 381.073 | 650.978 | Biaxl min | 11781 | 24 T 25 | 11781 |
| M104 | C14 | 1168.997 | 381.093 | 650.724 | Biaxl min | 11781 | 24 T 25 | 11781 |
| M105 | C14 | 664.247 | 216.544 | 488.096 | Biaxl min | 7854 | 16 T 25 | 7854 |

And given below table here shows the shear reinforcement for all the columns
Table 4.6.2 Shear Reinforcement

| Mem | Max Shear in Localy |  |  | Max Shear in Local z |  |  | Asv Req.$\mathrm{mm}^{2}$ | Link Size | Spacing cm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L/C | Value kN | Position m | L/C | Value kN | Position m |  |  |  |
| M73 | C14 | 20.630 | 3.000 | C14 | 108.373 | 0.000 | 0 | 10 | 7.1 |
| M74 | C14 | 19.002 | 15.000 | C14 | 121.263 | 0.000 | 0 | 10 | 7.1 |
| M75 | C14 | 18.936 | 15.000 | C14 | 121.072 | 0.000 | 0 | 10 | 7.1 |
| M76 | C14 | 13.692 | 15.000 | C14 | 94.359 | 0.000 | 0 | 10 | 7.1 |
| M77 | C14 | 20.441 | 3.000 | C14 | 109.669 | 0.000 | 0 | 10 | 7.1 |
| M78 | C14 | 13.025 | 3.000 | C14 | 129.665 | 0.000 | 0 | 10 | 7.1 |
| M79 | C14 | 2.409 | 12.000 | C14 | 140.819 | 0.000 | 0 | 10 | 7.1 |
| M80 | C14 | 2.784 | 15.000 | C14 | 140.641 | 0.000 | 0 | 10 | 7.1 |
| M81 | C14 | 10.056 | 15.000 | C14 | 133.761 | 0.000 | 0 | 10 | 7.1 |
| M82 | C14 | 11.689 | 15.000 | C14 | 95.251 | 0.000 | 0 | 10 | 7.1 |
| M83 | C14 | 1.159 | 15.000 | C14 | 118.629 | 0.000 | 0 | 10 | 7.1 |
| M84 | C14 | 0.497 | 12.000 | C14 | 141.833 | 0.000 | 0 | 10 | 7.1 |
| M85 | C14 | 141.236 | 0.000 | C14 | 0.218 | 0.000 | 0 | 10 | 7.1 |
| M86 | C14 | 0.374 | 12.000 | C14 | 128.890 | 0.000 | 0 | 10 | 7.1 |
| M87 | C14 | 0.310 | 12.000 | C14 | 141.095 | 0.000 | 0 | 10 | 7.1 |
| M88 | C14 | 0.699 | 12.000 | C14 | 141.237 | 0.000 | 0 | 10 | 7.1 |
| M89 | C14 | 1.134 | 15.000 | C14 | 109.496 | 0.000 | 0 | 10 | 7.1 |
| M90 | C14 | 1.159 | 15.000 | C14 | 118.629 | 0.000 | 0 | 10 | 7.1 |
| M91 | C14 | 0.497 | 12.000 | C14 | 141.833 | 0.000 | 0 | 10 | 7.1 |
| M92 | C14 | 0.374 | 15.000 | C14 | 141.237 | 0.000 | 0 | 10 | 7.1 |
| M93 | C14 | 0.310 | 12.000 | C14 | 141.095 | 0.000 | 0 | 10 | 7.1 |
| M94 | C14 | 0.699 | 12.000 | C14 | 141.237 | 0.000 | 0 | 10 | 7.1 |
| M95 | C14 | 1.134 | 15.000 | C14 | 109.496 | 0.000 | 0 | 10 | 7.1 |
| M96 | C14 | 20.441 | 3.000 | C14 | 109.669 | 0.000 | 0 | 10 | 7.1 |
| M97 | C14 | 13.025 | 3.000 | C14 | 129.665 | 0.000 | 0 | 10 | 7.1 |
| M98 | C14 | 2.409 | 12.000 | C14 | 140.819 | 0.000 | 0 | 10 | 7.1 |
| M99 | C14 | 2.784 | 15.000 | C14 | 140.641 | 0.000 | 0 | 10 | 7.1 |
|  |  |  |  |  |  |  |  |  |  |
| M100 | C14 | 10.056 | 15.000 | C14 | 133.761 | 0.000 | 0 | 10 | 7.1 |
| M101 | C14 | 11.689 | 15.000 | C14 | 95.251 | 0.000 | 0 | 10 | 7.1 |
| M102 | C14 | 20.630 | 3.000 | C14 | 108.373 | 0.000 | 0 | 10 | 7.1 |
| M103 | C14 | 19.003 | 15.000 | C14 | 121.263 | 0.000 | 0 | 10 | 7.1 |
| M104 | C14 | 18.936 | 15.000 | C14 | 121.072 | 0.000 | 0 | 10 | 7.1 |
| M105 | C14 | 13.692 | 15.000 | C14 | 94.359 | 0.000 | 0 | 10 | 7.1 |

### 4.7 Beam Design

Design Load for which beams are designed $=1.2(\mathrm{DL}+\mathrm{LL}-\mathrm{EQZ})$


Member 23 (Shear Reinforcement layout)


### 4.8 Slab Design

Slab 6, specified Design load = 1.2(DL+LL-EQZ)


Fig. 4.8.1 Showing Displacement Contour


Fig. 4.8.2 Result line graph showing displacement over the span


Fig. 4.8.3 Principal Major Stress (Top Reinforcement)


Fig. 4.8.4 Principal Minor Stress (Top Reinforcement)


Fig. 4.8.5 Principal Major Stress (Bottom reinforcement)


Fig. 4.8.6 Principal Minor Stress (Bottom Reinforcement)

### 4.9 Foundation Design

1. Foundation Type - Isolated
2. Soil Bearing Capacity $-230 \mathrm{kN} / \mathrm{m}^{2}$

### 4.9.1 Parameters for Design

| Unit Weight of Concrete | $25.00 \mathrm{kN} / \mathrm{m}^{3}$ |
| :--- | :--- |
| Strength of concrete | $25.00 \mathrm{~N} / \mathrm{mm}^{2}$ |
| Yield strength of concrete | $415.00 \mathrm{~N} / \mathrm{mm}^{2}$ |
| Minimum Bar Dia. | $\emptyset 12$ |
| Maximum Bar Dia. | $\emptyset 25$ |
| Minimum Bar Spacing | 50.00 mm |
| Maximum Bar Spacing | 500.00 mm |


| Load Combination/s- Service Stress Level |  |  |
| :---: | :---: | :---: |
| Load Combination <br> Number | Load Combination Title |  |
| 19 | DL+LL |  |
| 20 | DL+0.5LL+EQX |  |
| 21 | DL+0.5LL-EQX |  |
| 22 | DL+0.5LL+EQZ |  |
| 23 | DL+0.5LL-EQZ |  |
| Load Combination/s- Strength Level |  |  |
| Load Combination <br> Number | Load Combination Title |  |
| 19 | DL+LL |  |
| 20 | DL+0.5LL+EQX |  |
| 21 | DL+0.5LL-EQX |  |
| 22 | DL+0.5LL+EQZ |  |
| 23 | DL+0.5LL-EQZ |  |


| Applied Loads - Service Stress Level |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| LC | Axial <br> $(\mathrm{kN})$ | Shear X <br> $(\mathrm{kN})$ | Shear Z <br> $(\mathrm{kN})$ | Moment X <br> $(\mathrm{kNm})$ | Moment Z <br> $(\mathrm{kNm})$ |
|  | 879.951 | -8.592 | -8.821 | -8.600 | 8.316 |
| 20 | 828.023 | 7.556 | -7.570 | -7.212 | -49.791 |
| 21 | 660.207 | 10.415 | -4.611 | -4.293 | -52.564 |
| 22 | 827.390 | -7.384 | 7.468 | 49.751 | 7.006 |
| 23 | 659.574 | -4.524 | 10.427 | 52.671 | 4.233 |


| Applied Loads - Strength Level |  |  |  |  |  |
| :---: | :--- | :---: | :---: | :---: | :---: |
| LC <br> Axial <br> $(\mathrm{kN})$ | Shear X <br> $(\mathrm{kN})$ | Shear Z <br> $(\mathrm{kN})$ | Moment X <br> $(\mathrm{kNm})$ | Moment Z <br> $(\mathrm{kNm})$ |  |
|  | 879.951 | -8.592 | -8.821 | -8.600 | 8.316 |
| 20 | 828.023 | 7.556 | -7.570 | -7.212 | -49.791 |
| 21 | 660.207 | 10.415 | -4.611 | -4.293 | -52.564 |
| 22 | 827.390 | -7.384 | 7.468 | 49.751 | 7.006 |
| 23 | 659.574 | -4.524 | 10.427 | 52.671 | 4.233 |

### 4.9.2 Calculations for Design

## Size of Footing

Initial Length : $\mathrm{L}_{\mathrm{o}}$ -
1.00 m

Initial Width : Wo -
1.00 m

Initial length and width area: $\mathrm{A}_{\mathrm{o}}$ -
$\mathrm{L}_{\mathrm{o}} * \mathrm{~W}_{\mathrm{o}}=1.00 \mathrm{~m}^{2}$
Min. required area for bearing pressure : $\mathrm{A}_{\text {min }}$ -
$\mathrm{P} / \mathrm{q} \max =3.859 \mathrm{~m}^{2}$

Final dimensions for design

Length, $\mathrm{L}_{2}-3.35 \mathrm{~m} \quad$ Governing Load Case : 20
Width, $\mathrm{W}_{2}$ -
3.35 m Governing Load Case : 20

Area, $\mathrm{A}_{2}$ -
$11.223 \mathrm{~m}^{2}$

## Check For Stability Against Overturning And Sliding

| - | Factor of safety against sliding | Factor of safety against overturning |  |
| :---: | :---: | :---: | :---: |
| Load Case <br> No. | Along X- <br> Direction | Along Z- <br> Direction | About X-Direction | About Z-Direction

Critical load case and the governing factor of safety for overturning and sliding

Critical Load Case for Sliding along X-Direction :
Governing Disturbing Force :
Governing Restoring Force :
Minimum Sliding Ratio for the Critical Load Case :
Critical Load Case for Overturning about X-Direction :
Governing Overturning Moment :
Governing Resisting Moment :
Minimum Overturning Ratio for the Critical Load Case :
20.623 kN
700.039 kN
33.945 kN

21
$-374.045 \mathrm{kNm}$
2345.088 kNm
6.270

## Critical load case and the governing factor of safety for overturning and sliding

| Critical Load Case for Sliding along Z-Direction : | 21 |
| :--- | :--- |
| Governing Disturbing Force : | -117.561 kN |
| Governing Restoring Force : | 700.039 kN |
| Minimum Sliding Ratio for the Critical Load Case : | 5.955 |
| Critical Load Case for Overturning about Z-Direction : | 21 |
| Governing Overturning Moment : | -67.960 kNm |
| Governing Resisting Moment : | 2345.088 kNm |
| Minimum Overturning Ratio for the Critical Load Case : | 34.507 |

## Check Trial Depth against moment (w.r.t. X Axis)

| Critical Load Case | $=\# \mathbf{2 0}$ |  |  |
| ---: | :--- | :--- | :--- |
| Effective Depth $=$ | D-(cc $\left.+0.5 \times d_{b}\right)$ | $=0.449$ | m |
| Effective End Depth $=$ | Initial End Depth $-\mathrm{D}-\left(\mathrm{cc}+0.5 \times d_{b}\right)$ | $=0.256$ | m |
| Effective Width of Equivalent Rectangle $=$ | Col. Width $+($ Footing Width - Col. <br> Width $) / 8.0$ | $=0.944$ | m |
| Governing moment $\left(\mathrm{M}_{\mathrm{u}}\right)$ |  | $=601.771$ | kNm |

As Per IS 4562000 ANNEX G G-1.1C

$$
\begin{array}{cccc}
\text { Limiting Factor1 }\left(\mathrm{K}_{\mathrm{umax}}\right)= & \frac{700}{\left(1100+0.87 \times \mathrm{f}_{\mathrm{y}}\right)} & =0.479107 \\
\text { Limiting Factor2 }\left(R_{\mathrm{umax}}\right)= & 0.36 \times \mathrm{f}_{\mathrm{ck}} \times \mathrm{k}_{\mathrm{umax}} \times(1-0.42 \times \text { humax }) & =3444.291146 & \mathrm{kN} / \mathrm{m} 2 \\
\text { ent Of Resistance }\left(\mathrm{M}_{\mathrm{umax}}\right)= & \mathrm{R}_{\text {umax }} \times{\mathrm{BB} \times \mathrm{d}_{\mathrm{e}}}^{2} & =655.302109 & \mathrm{kNm} \\
\mathrm{M}_{\mathrm{u}}<=\mathrm{M}_{\mathrm{umax}} & \text { hence, safe } & &
\end{array}
$$

| Critical Load Case | = \#20 |  |  |
| :---: | :---: | :---: | :---: |
| Effective Depth = | D - $\left(\mathrm{cc}+0.5 \times \mathrm{d}_{\mathrm{b}}\right)$ | $=0.449$ | m |
| Effective End Depth |  | $=0.256$ | m |
| Effective Width |  | $=0.944$ | m |
| Governing moment $\left(M_{u}\right)=$ |  | $=486.922$ | kNm |
| As Per IS 4562000 ANNEX G G-1.1C |  |  |  |
| Limiting Factor1 $\left(\mathrm{K}_{\text {umax }}\right)=$ | $\frac{700}{\left(1100+0.87 \times f_{y}\right)}$ | $=0.479107$ |  |
| Limiting Factor2 ( $\left.\mathrm{R}_{\mathrm{umax}}\right)=$ | $0.36 \times \mathrm{f} \mathrm{ck}^{\times \mathrm{K}_{\text {umax }} \times(1-0.42 \times \text { humax })}$ | $=3444.291146$ | kN/m2 |
| Limit Moment Of Resistance $\left(\mathrm{M}_{\text {umax }}\right)=$ | $\mathrm{R}_{\text {umax }} \times \mathrm{B} \times \mathrm{de}_{\mathrm{e}}{ }^{2}$ | $=655.302109$ | kNm |
| $M_{u}<=M_{u m a x}$ | hence, safe |  |  |

### 4.9.3 Foundation Geometry for all footings:

Table 4.9.3.1 Foundation Geometry

| Footing No. | $\begin{gathered} \text { Grovp } \\ \text { ID } \end{gathered}$ | Foundation Geometry |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| - | - | Length | Width | Thickne <br> ss | Slope End Thickne ss |
| 2 | 1 | 2.950 mm | 2.950 mm | 0.455 m | 0.212 mm |
| 3 | 2 | 3.350 mm | 3.350 mm | 0.505 mm | 0.312 mm |
| 4 | 3 | 3.350 mm | 3.350 mm | 0.505 mm | 0.312 mm |
| 5 | 4 | 3.050 mm | 3.050 mm | 0.455 mm | 0.262 mm |
| 43 | 5 | 2.950 mm | 2.950 mm | 0.455 mm | 0.212 mm |
| 44 | 6 | 3.400 mm | 3.400 mm | 0.555 m | 0.312 mm |
| 45 | 7 | 3.450 mm | 3.450 mm | 0.555 mm | 0.312 mm |
| 46 | 8 | 3.450 mm | 3.450 mm | 0.555 m | 0.312 mm |
| 47 | 9 | 3.450 mm | 3.450 mm | 0.555 mm | 0.362 mm |
| 4 S | 10 | 3.050 mm | 3.050 mm | 0.455 mm | 0.262 mm |
| 85 | 1.1 | 3.050 mm | 3.050 mm | 0.455 mm | 0.262 mm |
| 86 | 12 | 3.450 mm | 3.450 mm | 0.555 m | 0.312 mm |
| 87 | 13 | 3.450 mm | 3.450 mm | 0.555 m | 0.312 mm |
| 88 | 14 | 3.450 mm | 3.450 mm | 0.555 m | 0.312 mm |
| 89 | 15 | 3.450 mm | 3.450 mm | 0.555 m | 0.312 mm |
| 90 | 16 | 3.200 mm | 3.200 mm | 0.455 m | 0.262 mm |
| 127 | 17 | 3.050 mm | 3.050 mm | 0.455 m | 0.262 mm |
| 12 S | 13 | 3.450 mm | 3.450 mm | 0.555 m | 0.312 mm |
| 129 | 19 | 3.450 mm | 3.450 mm | 0.555 m | 0.312 mm |
| 130 | 20 | 3.450 mm | 3.450 mm | 0.555 mm | 0.312 mm |
| 131 | 21 | 3.450 mm | 3.450 mm | 0.555 mm | 0.312 mm |
| 132 | 22 | 3.200 mm | 3.200 mm | 0.455 m | 0.262 mm |
| 169 | 23 | 2.850 mm | 2.850 mm | 0.405 mm | 0.162 m |
| 170 | 24 | 3.300 mm | 3.300 mm | 0.505 m | 0.312 mm |
| 171 | 25 | 3.450 mm | 3.450 mm | 0.555 mm | 0.312 mm |
| 172 | 26 | 3.450 mm | 3.450 mm | 0.555 mm | 0.312 mm |
| 173 | 27 | 3.300 mm | 3.300 mm | 0.505 mm | 0.312 mm |
| 174 | 23 | 2.700 mm | 2.700 mm | 0.405 mm | 0.212 mm |
| 212 | 29 | 2.850 mm | 2.850 mm | 0.405 mm | 0.162 mm |
| 213 | 30 | 2.900 mm | 2.900 mm | 0.405 mm | 0.212 mm |
| 214 | 31 | 2.900 mm | 2.900 mm | 0.405 mm | 0.212 mm |
| 215 | 32 | 2.700 mm | 2.700 mm | 0.405 mm | 0.212 mm |

### 4.9.4 Foundation $R / F$ of whole building

Table 4.9.4.1 Foundation reinforcement

| Footing No. | Footing Reinforcement |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| - | Bottom Reinforcement( $\mathrm{M}_{z}$ ) | Bottom Reinforcement( $\mathrm{M}_{\mathrm{x}}$ ) | Top Reinforcement( $\mathrm{M}_{z}$ ) | Top Reinforcement( $\mathrm{M}_{\mathrm{x}}$ ) |
| 2 | Ø12@ $140 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $90 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $175 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $235 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 3 | $\emptyset 12$ @ $105 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $00 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $130 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $200 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 4 | $\emptyset 12$ @ $105 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $00 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $130 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $200 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 5 | $\emptyset 12$ @ $130 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 90 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $170 \mathrm{~mm} \mathrm{c/c}$ | Ø12@ $225 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 43 | $\emptyset 12$ @ $140 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $90 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $175 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 235 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 44 | $\emptyset 12 @ 95 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $70 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $125 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $205 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 45 | Ø12@ $100 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $75 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $135 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $205 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 46 | Ø12@ $100 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $75 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $135 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $205 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 47 | $\emptyset 12 @ 100 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $75 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 120 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $205 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 48 | $\emptyset 12 @ 130 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $90 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $170 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $225 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 85 | Ø12@ $130 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $85 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $150 \mathrm{~mm} \mathrm{c/c}$ | Ø12@ $225 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 86 | $\emptyset 12$ @ $100 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $75 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $135 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $205 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 87 | $\emptyset 12$ @ $95 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $75 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $135 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $205 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 88 | Ø12@ $95 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $75 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $135 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $205 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 89 | Ø12@ $100 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $75 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $135 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $205 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 90 | Ø12@ $110 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $00 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $150 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $235 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 127 | $\emptyset 12$ @ $130 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $90 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $150 \mathrm{~mm} \mathrm{c/c}$ | $\emptyset 12$ @ $225 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 128 | $\emptyset 12 @ 100 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $75 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $135 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $205 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 129 | Ø12@ $95 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $75 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $135 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $205 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 130 | $\emptyset 12$ @ $95 \mathrm{~mm} \mathrm{c/c}$ | Ø12@ $75 \mathrm{~mm} \mathrm{c/c}$ | $\emptyset 12$ @ $135 \mathrm{~mm} \mathrm{c/c}$ | $\emptyset 12$ @ $205 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 131 | Ø12@ $100 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $75 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $135 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $205 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 132 | Ø12 @ $110 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | Ø12@ $80 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12$ @ $150 \mathrm{~mm} \mathrm{c/c}$ | Ø12@ $235 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |


| 169 | $\emptyset 12 @ 195 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 105 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 270 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 270 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| :--- | :---: | :---: | :---: | :---: |
| 170 | $\emptyset 12 @ 115 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 85 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 150 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 210 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 171 | $\emptyset 12 @ 100 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 75 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 135 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 205 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 172 | $\emptyset 12 @ 100 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 75 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 135 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 205 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 173 | $\emptyset 12 @ 105 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 80 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 150 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 210 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 174 | $\emptyset 12 @ 235 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 135 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 255 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 255 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 212 | $\emptyset 12 @ 195 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 105 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 270 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 270 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 213 | $\emptyset 12 @ 145 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 95 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 195 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 275 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 214 | $\emptyset 12 @ 145 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 95 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 195 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 275 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| 215 | $\emptyset 12 @ 235 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 135 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 255 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | $\emptyset 12 @ 255 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |

### 4.10 Cost Analysis

### 4.10.1 Construction cost

Table 4.10.1.1 Built-Up Area of 1 Building

| Over-all Built-Up area | $21824 \mathrm{ft}^{2}$ |
| :--- | :--- |
| Ground Floor | $3704 \mathrm{ft}^{2}$ |
| First Floor | $3624 \mathrm{ft}^{2}$ |
| Second Floor | $3624 \mathrm{ft}^{2}$ |
| Third Floor | $3624 \mathrm{ft}^{2}$ |
| Fourth Floor | $3624 \mathrm{ft}^{2}$ |
| Fifth Floor | $3624 \mathrm{ft}^{2}$ |

$$
\text { -回 } \mathbb{E}
$$




Fig. 4.10.1.1 Model of Ground floor of building


Fig. 4.10.1.2 Model of building complex

Table 4.10.1.2 Estimate of one Building

| S. No. | Family \& Category | Name of Material | Area of Material | Cost of Material(₹) | Overall Cost |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Floor Tile 24*48 (Ground Floor) :1 | Floor Tile $24 * 48$ | 3704 SF | 250 | ₹ 926000 |
| 2 | Floor Tile 24 X 48 :5 | Floor Tile 24 X 48 | 18120 SF | 300 | ₹ 5436000 |
| 3 | $\begin{aligned} & \text { Exterior wall 8" } \\ & : 108 \end{aligned}$ | Concrete <br> Masonry <br> Units | 4770 SF | 140 | ₹ 667800 |
| 4 | $\begin{aligned} & \text { Interior Wall 6" } \\ & : 162 \end{aligned}$ | Common Brick | 7464 SF | 110 | ₹ 821040 |
| 5 | Generic Basic Roof 6":1 | Default Roof | 3624 SF | 300 | ₹ 1087200 |
| 6 | $\begin{aligned} & \text { Column } \\ & 24 " \text { X } 24 ": 192 \end{aligned}$ | Default Wall | 16512 SF | 110 | ₹ 1816320 |
| 7 | Flush Door: $\text { 34"X 84" } 60$ | Door Frame | 1380 SF | 200 | ₹ 276000 |
| 8 | Flush Door: $34 " X 84 ": 60$ | Door Panel | 2700 SF | 200 | ₹ 540000 |
| 9 | $\begin{aligned} & \text { Panel Door: } \\ & 34 " \text { X } 84 ": 36 \end{aligned}$ | Door Frame | 828 SF | 280 | ₹ 231840 |
| 10 | Panel Door: $34 " \text { X 84" : } 36$ | Door Panel | 1800 SF | 280 | ₹ 504000 |
| 11 | Glass : 192 | Glass | 4608 SF | 90 | ₹ 414720 |
| 12 | Sash : 96 | Sash | 1632 SF | 180 | ₹ 293760 |
| 13 | Trim : 96 | Trim | 960 SF | 230 | ₹ 220800 |
|  |  |  |  | Total | ₹ 13235480 |

Table 4.10.1.3 Estimate of all buildings

| S. <br> No. | Family \& Category | Name of Material | Area of Material | Cost of Material(₹) | Overall Cost |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Floor Tile 24*48 (Ground Floor) :4 | $\begin{aligned} & \hline \text { Floor Tile } \\ & 24 * 48 \end{aligned}$ | 14816 SF | 250 | ₹ 3704000 |
| 2 | $\begin{aligned} & \text { Floor Tile } \\ & 24 \text { X } 48: 20 \end{aligned}$ | $\begin{aligned} & \text { Floor Tile } \\ & 24 \text { X } 48 \end{aligned}$ | 72480 SF | 300 | ₹ 21744000 |
| 3 | Exterior wall 8" $\text { : } 432$ | Concrete <br> Masonry <br> Units | 19080 SF | 140 | ₹ 2671200 |
| 4 | $\begin{aligned} & \text { Interior Wall 6" } \\ & : 648 \end{aligned}$ | Common Brick | 29856 SF | 110 | ₹ 3284160 |
| 5 | Generic Basic Roof 6": 4 | Default Roof | 14496 SF | 300 | ₹ 4348800 |
| 6 | $\begin{aligned} & \text { Column } \\ & 24 " \text { X } 24 ": 768 \end{aligned}$ | Default Wall | 66048 SF | 110 | ₹ 7265280 |
| 7 | Flush Door: $34 " X 84 ": 240$ | Door Frame | 5520 SF | 200 | ₹ 1104000 |
| 8 | Flush Door: $34 " X 84 ": 240$ | Door Panel | 10800 SF | 200 | ₹ 2160000 |
| 9 | Panel Door: $34 " \text { X 84" : } 144$ | Door Frame | 3312 SF | 280 | ₹ 927360 |
| 10 | Panel Door: $34 " \text { X 84" : } 144$ | Door Panel | 7200 SF | 280 | ₹ 2016000 |
| 11 | Glass : 768 | Glass | 18432 SF | 90 | ₹ 1658880 |
| 12 | Sash : 384 | Sash | 6528 SF | 180 | ₹ 1175040 |
| 13 | Trim : 384 | Trim | 3840 SF | 230 | ₹ 883200 |
|  |  |  |  | Total | ₹ 52941920 |

Table 4.10.1.4 Total Constructing Cost of all Buildings

| Constructing Cost | ₹ 52941920 |
| :--- | :--- |
| Painting cost per sq. ft. | ₹ 30 |
| Total painting cost | ₹ 5545440 |
| Total constructing cost | ₹ 58487360 |
| $1 \%$ of total cost ( Tools \& Tackles) | ₹ 584873.60 |
| $2 \%$ of total cost (Water Charges) | ₹ 1169747.20 |
| $5 \%$ of total cost (Sanitary fittings) | ₹ 2924368 |
| $10 \%$ of total cost (Contractor’s Profit) | ₹ 5848736 |
| $30 \%$ of total cost17546208 (Labor charges ) | ₹ 17546208 |
| Total Construction Cost of whole Project | ₹ 86561292.8 |

## CHAPTER 5 <br> CONCLUSION

### 5.1 General

STAAD PRO gives us reinforcement requirement for concrete members and the project contains many members all designed as per IS: 456 (2000).

1. Max. Hogging and sagging moments are calculated for the design load and other active load cases. And every section is designed to resist the critical hogging and sagging moment.
2. Shear R/F is calculated to resist both S.F \& torsional moments.
2.1 Max. Deflection at different nodes < 30 mm .
2.2 In shear \& flexure structural components are safe of the building.
3. Increment in the quantity of analysis tools is an indication to the expanding significance of manageable plan in engineering and the need to enhance building execution is appropriate for conveying the sort of data that can be utilized to improve plan and building execution. REVIT arch. Systematizes the hard work of activities like Material Takeoff, Schedule/Quantities etc. whilst taking and coordinating data in the documents set.

Total Construction Cost of whole Project $=₹ 86561292.8$
Total Project Duration = 524 days
4. Construction of structure utilizing Traditional path ends up being uneconomical and expends additional time with numerous complexibility and gigantic mistake which affects actual execution of the Project. Customary way for planning doesn't sub separate the primary task like over allocation of assets, inappropriate judgment of assets for specific activities and so forth.

### 5.2 Future Scope

An effective construction project management must have varied plans \& advanced concepts to benefit in advancing and managing numerous projects. It offers the basis for a career path in the construction industry and offers a good understanding of the theoretic ideas of construction practices.

And since technology is changing always and advancing similarly it is changing in the architecture, civil engineering or design field also. And since software play a very major role so having good knowledge of software like AutoCAD, STAAD Pro, 3ds Max, Revit, Primavera, Rhino etc. can help in a great way.

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## APPENDIX A

## A. 1 STAAD INPUT FILE

STAAD SPACE

START JOB INFORMATION
ENGINEER DATE 10-Feb-19
END JOB INFORMATION
INPUT WIDTH 79
SET PRINT 5
UNIT METER KN
JOINT COORDINATES
$23.9725300 ; 37.9450500 ; 411.917600 ; 515.890100 ; 83.9725330$ 0;
97.945053 0; 1011.917630 ; 1115.89013 0; 143.9725360 ; 157.9450560 ;
$1611.917660 ; 1715.890160 ; 203.9725390 ; 217.9450590 ; 2211.917690$;
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41 15.8901 18 0; 4300 3.97253; 443.972530 3.97253; 457.945050 3.97253;
4611.91760 3.97253; 4715.890103 .97253 ; 4819.86260 3.97253;

4903 3.97253; 503.972533 3.97253; 517.9450533 .97253 ;
5211.91763 3.97253; 5315.89013 3.97253; 5419.86263 3.97253;

5506 3.97253; 563.972536 3.97253; 577.945056 3.97253;
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6109 3.97253; 623.972539 3.97253; 637.945059 3.97253;
64 11.9176 9 3.97253; 6515.89019 3.97253; 6619.86269 3.97253;
67012 3.97253; 683.9725312 3.97253; 697.94505123 .97253 ;
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73015 3.97253; 743.9725315 3.97253; 757.9450515 3.97253;
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## MEMBER INCIDENCES

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## ELEMENT PROPERTY

576 TO 701 THICKNESS 0.15
DEFINE MATERIAL START
ISOTROPIC CONCRETE
E 2.17184e+007
POISSON 0.17
DENSITY 23.6158
ALPHA 5e-006
DAMP 0.05
TYPE CONCRETE
STRENGTH FCU 27578.9
END DEFINE MATERIAL
MEMBER PROPERTY AMERICAN

2 TO 47 TO 912 TO 1417 TO 1922 TO 2427 TO 2967 TO 96133 TO 162199 200 TO 228265 TO 294332 TO 334337 TO 339342 TO 344347 TO 349352 TO 354 357 TO 359398 TO 401404 TO 407410 TO 413416 TO 419422 TO 425 428 TO 431433 TO 540542 TO 545548 TO 551554 TO 557560 TO 563 566 TO 569572 TO 575 PRIS YD 0.3 ZD 0.3 32 TO 3538 TO 4144 TO 4750 TO 5356 TO 5962 TO 6597 TO 132163 TO 198 229 TO 264295 TO 330362 TO 365368 TO 371374 TO 377380 TO 383 -

386 TO 389392 TO 395 PRIS YD 0.6 ZD 0.6
CONSTANTS
BETA 90 MEMB 166
MATERIAL CONCRETE ALL
SUPPORTS
2 TO 543 TO 4885 TO 90127 TO 132169 TO 174212 TO 215 FIXED
DEFINE 1893 LOAD
ZONE 0.075 RF 5 I 1 SS 2 ST 1 DM 0.05

## SELFWEIGHT 1

FLOOR WEIGHT
YRANGE 318 FLOAD 3.75
YRANGE 315 FLOAD 2
MEMBER WEIGHT
2 TO 47 TO 912 TO 1417 TO 1922 TO 2467717276778182868791265 269270274275279280284285289332 TO 334337 TO 339342 TO 344347 -

348 TO 349352 TO 354398401404407410413416419422425433438439 -
444445450451456457462469474475480481486487492493498505510 -
511516517522523528529534542545548551554557560563566 -
569 UNI 19.15
27 TO 299296290294357 TO 359428431463468499504535540572575 UNI 8 68 TO 7073 TO 7578 TO 8083 TO 8588 TO 9093 TO 95133 TO 162199 TO 228 266 TO 268271 TO 273276 TO 278281 TO 283286 TO 288291 TO 293399400 405406411412417418423424429430434 TO 437440 TO 443446 TO 449 452 TO 455458 TO 461464 TO 467470 TO 473476 TO 479482 TO 485 -

488 TO 491494 TO 497500 TO 503506 TO 509512 TO 515518 TO 521 524 TO 527530 TO 533536 TO 539543544549550555556561562567568 573574 UNI 11.8

DEFINE WIND LOAD
TYPE 1 WIND 1
INT 0.750 .90 .991 .11 .25 1.37 HEIG $36 \begin{array}{llll}6 & 12 & 15 & 18\end{array}$
EXP 1 JOINT 2 TO 58 TO 1114 TO 1720 TO 2326 TO 2932 TO 3538 TO 4143 44 TO 210212 TO 215218 TO 221224 TO 227230 TO 233236 TO 239242 TO 245 248 TO 251

LOAD 1 LOADTYPE Seismic TITLE EQX
1893 LOAD X 1
LOAD 2 LOADTYPE Seismic TITLE EQZ
1893 LOAD Z 1
LOAD 3 LOADTYPE Dead TITLE DL
SELFWEIGHT Y-1
FLOOR LOAD
YRANGE 318 FLOAD -3.75 GY
MEMBER LOAD
2 TO 47 TO 912 TO 1417 TO 1922 TO 2467717276778182868791265 269270274275279280284285289332 TO 334337 TO 339342 TO 344347 348 TO 349352 TO 354398401404407410413416419422425433438439 444445450451456457462469474475480481486487492493498505510 511516517522523528529534542545548551554557560563566 569 UNI GY - 19.15

27 TO 299296290294357 TO 359428431463468499504535540572 575 UNI GY - 8

68 TO 7073 TO 7578 TO 8083 TO 8588 TO 9093 TO 95133 TO 162199 TO 228 266 TO 268271 TO 273276 TO 278281 TO 283286 TO 288291 TO 293399400 405406411412417418423424429430434 TO 437440 TO 443446 TO 449 452 TO 455458 TO 461464 TO 467470 TO 473476 TO 479482 TO 485 488 TO 491494 TO 497500 TO 503506 TO 509512 TO 515518 TO 521 -

524 TO 527530 TO 533536 TO 539543544549550555556561562567568 -
573574 UNI GY -11.8
ELEMENT LOAD
576 TO 701 PR LY -2
LOAD 4 LOADTYPE Live REDUCIBLE TITLE LL
FLOOR LOAD
YRANGE 315 FLOAD -4 GY
LOAD 5 LOADTYPE Roof Live REDUCIBLE TITLE RLL
FLOOR LOAD
YRANGE 1618 FLOAD -2 GY
LOAD 6 LOADTYPE Wind TITLE WL X
WIND LOAD X 1 TYPE 1 YR 318
LOAD 7 LOADTYPE Wind TITLE WL -X
WIND LOAD X -1 TYPE 1 YR 318
LOAD 8 LOADTYPE Wind TITLE WL Z
WIND LOAD Z 1 TYPE 1 YR 318
LOAD 9 LOADTYPE Wind TITLE WL -Z
WIND LOAD Z -1 TYPE 1 YR 318
**********************
**********************
***Load Combination for frame design
LOAD COMB 11 1.2(DL+LL+EQX)
11.231 .241 .2

LOAD COMB 12 1.2(DL+LL-EQX)
$11.231 .24-1.2$
LOAD COMB 13 1.2(DL+LL+EQZ)
21.231 .241 .2

LOAD COMB 14 1.2(DL+LL-EQZ)
$21.231 .24-1.2$
LOAD COMB 19 DL+LL
31.041 .0

LOAD COMB 20 DL+0.5LL+EQX
11.031 .041 .0

LOAD COMB 21 DL+0.5LL-EQX
$11.031 .04-1.0$
LOAD COMB 22 DL+0.5LL+EQZ
21.031 .041 .0

LOAD COMB 23 DL+0.5LL-EQZ
$21.031 .04-1.0$
PERFORM ANALYSIS
START CONCRETE DESIGN
CODE INDIAN
FC 25000 ALL
FYMAIN 415000 ALL
DESIGN BEAM 2 TO 47 TO 912 TO 1417 TO 1922 TO 2427 TO 2967 TO 96133 -
134 TO 162199 TO 228265 TO 294332 TO 334337 TO 339342 TO 344347 TO 349 -
352 TO 354357 TO 359398 TO 401404 TO 407410 TO 413416 TO 419 -
422 TO 425428 TO 431433 TO 540542 TO 545548 TO 551554 TO 557 -
560 TO 563566 TO 569572 TO 575
DESIGN COLUMN 32 TO 3538 TO 4144 TO 4750 TO 5356 TO 5962 TO 65 -
97 TO 132163 TO 198229 TO 264295 TO 330362 TO 365368 TO 371374 TO 377 -
380 TO 383386 TO 389392 TO 395
DESIGN ELEMENT 576 TO 701
CONCRETE TAKE
FYSEC 415000 ALL
MAXMAIN 16 ALL
MAXSEC 10 ALL
START BAR COMBINATION
MD1 10 ALL
MD2 12 ALL
END BAR COMBINATION
MINMAIN 12 ALL

MINSEC 8 ALL
RATIO 4 ALL
REINF 0 ALL
END CONCRETE DESIGN
PERFORM ANALYSIS
FINISH

