# FEASIBILITY OF SIDEWALK ALONG THE AMBALA-SHIMLA 

 NATIONAL HIGHWAY NO.-5 AT SHOGHI, SHIMLA, HIMACHAL PRADESH: DESIGN \& ANALYSIS
## A PROJECT

Submitted in partial fulfillment of the requirements for the award of the degree of

## BACHELOR OF TECHNOLOGY

IN
CIVIL ENGINEERING
Under the supervision of
Mr. Ashish Kumar \& Mr. Mani Mohan
By
Akshay Sharma (111649)
Pankaj Sharma (111673)
Jigme Wangdi (111692)
to


JAYPEE UNIVERSITY OF INFORMATION TECHNOLOGY

May, 2015

## CERTIFICATE

This certify that the work which is being presented in the project title "FEASIBILITY OF SIDEWALK ALONG THE AMBALA-SHIMLA NATIONAL HIGHWAY NO. -5 AT SHOGHI, SHIMLA, HIMACHAL PRADESH: DESIGN AND ANALYSIS" in partial fulfillment of the requirements for the award of the degree of Bachelor of technology and submitted in Civil Engineering Department, Jaypee University of Information Technology, Waknaghat is an authentic record of work carried out by Mr.Akshay Sharma(111649), Mr.Pankaj Sharma(111673) and Mr.Jigme Wangdi (111692) during a period from August 2014 to May2015 under the supervision of Mr. Ashish Kumar and Mr. Mani Mohan, Assistant Professors, Civil Engineering Department, Jaypee University of information Technology, Waknaghat.

The above statement made is correct to the best of my knowledge.

Date:- $\qquad$

Prof. Dr. Ashok Kumar Gupta
Professor \& Head of Department
Civil Engineering Department
JUIT Waknaghat

Mr. Mani Mohan
Assistant Professor
Civil Engineering Department
JUIT Waknaghat


#### Abstract

ACKNOWLEDGEMENT

This report would not have been possible without the essential and gracious support of Mr. Ashish Kumar. His willingness to motivate us contributed tremendously to our report. We also would like to thank him for giving us his valuable time, showing us the path to achieve our objectives and goals and for being there whenever we needed his expert guidance.

Also, we are highly grateful for the support and guidance of Mr. Mani Mohan who guided us in the absence of Mr. Ashish Kumar. He not only guided us but also provide us with unique and efficient solutions whenever we were in problem.

Besides, we would like to thank our Head of Department Prof. Dr. Ashok Kumar Gupta for providing us good environment and facilities to complete this project. Also we would like to take this opportunity to thank Jaypee University of Information Technology for offering this project.


Finally, we would like to thank our faculty members, lab assistants,family and friends for their understandings and supports towards us for completing this report.

Date: -


#### Abstract

From several years Shoghi is in great need of a parking facility and facility for pedestrians to walk upon. Our project 'Design of sidewalk at Shoghi' is a project that will not only addresses to these problems but also challenges us to apply our knowledge gained by us in the previous year's along with gaining of on-site work experience.

In the first chapter of this report we have given a brief introduction about Shoghi, its problems and possible solutions we have tried to find out. Also here we have discussed about the code IRC-103-1988 and which we have followed thus making the guidelines from the code as our base for the project. The second chapter gives us the details of the surveys which were performed by us. We have conducted both photographic and total station survey. Photographic survey has given us the fair idea of the problems faced by pedestrians and from the total station survey we collected data points that helped us to make a layout of the 1.1 km long stretch.

In the third chapter the procedure for making the layout of the stretch by the use of software's likes AutoCAD and MS-Excel has been provided. The layouts laid the foundation of the designing part of the project where we plotted the sidewalk as well as came to know about the types of supports by allocation of concrete footings along the side walk. The fourth chapter of this report contains the designing and analysis of the sections chosen by us to serve as the sidewalk using STAAD.Pro and MACROS feature of MS-Excel. Initially, upto Cross-Section No. 73 we designed steel sidewalk and for the rest of the stretch we used concrete sidewalk.


In the fifth chapter we have provided the estimate and cost analysis for carrying out the whole project and in final sixth chapter we have recommended some amendments that can be carried out for more safety of pedestrians.
Finally the results and discussions are drawn and the project is brought to its conclusion.

KEYWORDS:-AutoCAD, Concrete Sidewalk, MACROS, STAAD.Pro, Steel Sidewalk, Total Station Survey.

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## CHAPTER-1

## INTRODUCTION

## 1. 1 SHOGHI

Shoghi is a small suburb of Shimla, Himachal Pradesh, India. It is about 13 kilometers before Shimla on the Ambala Shimla national highway (NH-22). The road to the Taradevi temple (hilltop) goes from here which is about 5 km . Shoghi is also famous for bus halts for food as there are many dhabas (local name for food outlets) here. HIMUDA (Himachal Pradesh Urban Development Authority) has also constructed many flats here.

Nestled in the quaint, lush, green hills of Himachal Pradesh just 13 kilometers short of Shimla (The queen of hills), captivating building blocks of pinks and yellows with sloping tin roofs add a touch of natural grandeur to the picturesque surroundings. As you veer off the national highway towards the blocks, you realise you are entering the Housing Board Colony at Shoghi.

The colony was set up in the cozy hamlet of Shoghi in early 2001 by HIMUDA for meeting the housing needs of so many people. Not only accessible, the colony is far from the madding crowd situated on a knoll overlooking hills rising one after another to meet the insurmountable skies from a deep vale just across the road. You can go to Shoghi, and back to nature, without running into traffic jams, a characteristic of Shimla.

But over the years, the colony has lost most of its charm. The metalled road gives way to streets of cobbled stones, as your huffing and panting car wheezes its way up the hillock towards the rising blocks of flats.

Look down the slopes, along the colony streets, and you find the greenery suffocating under the thick layers of rubbish. Carelessly tossed wrappers of potato chips, aluminum foils and empty soda bottles not only narrate the tales of not-so-quiet evenings enjoyed with drinks, but also of sheer disrespect for the nature and inability of the authorities to
prevent the littering. The housing board society is now making attempts to clean up the mess, but the dirty picture's end is nowhere in sight.

It doesn't take you much time to realise that the colony has been left to fend for itself otherwise also. The concrete road signs, spelling out the location of the blocks, too seem to have crooked under their own weight. Security too is an issue. The colony precincts have not been demarcated; and in the absence of fencing, it's free for all. Water meters are stolen, and the open spaces in the campus have metamorphosised themselves into free public parking lots for the "outsiders".

Shoghi offers a beautiful option for a stay near Shimla with lots of nature activities. ${ }^{[8]}$

### 1.2 PROBLEMS AT SHOGHI

The main problem at Shoghi is from housing board colony gate-2 to Shimla bypass for heavy vehicles which is of 1.1 km stretch, within this stretch there is H.P.C.L (Hindustan Petroleum Corporation Limited) Shimla depot, police barrier, primary health center, a Government School, entrance gate towards Hosing Board colony, market place which contains taxi stand, Bus stand, DAV Public School and various kinds of shops and dhabas. For all these places to visit walking is a prime mode transport for the locals. In this stretch there are ample of space for the people to walk but there are always plenty of vehicles parked on the road and other available space making it


Fig.1.1 People walking on carriage way difficult and forcing people to walk on the carriage way.

Usually on this road, vehicles travel at an average speed of $50 \mathrm{~km} / \mathrm{h}$ and people walking along the road risks their life increasing the probability of accidents. Shimla being the hot-spot for tourists and trekkers the vehicle density on NH-22 is increasing day by day leading to the congestion on NH-22 and the authorities at Shimla tried to relieve this congestion by making a bypass at shoghi via Mehli for the heavy vehicles, at that time Shoghi was not that populated and vehicle density was also not that high but now both have drastically increased.

As there is no proper facility to walk and cross the road, it makes unsafe for the people.


Fig.1.2 Bypass road for heavy vehicles


Fig.1.3 Traffic jams at Bypass road at Shoghi

### 1.3 ABOUT THE PROJECT

In this project we have designed the side walk. Since people walking towards their daily work and destination faces lots of problem and the safety of the people is the biggest concern we decided to take up our final year project on side walk design. The foot path we designed is a raised foot path of 30 cm from the carriage way level. Also we have
provided proper openings where ever necessary. For the people to cross from one road to another road we decided to provide zebra crossings and speed breaker to lower the speed of the moving vehicles. In this project we followed the IS 103-1988 for the guidelines.

### 1.3.1 OBJECTIVES

- To provide a safe walking area to the pedestrians of Shoghi.
- To design a feasible and economical sidewalk that can bear maximum load and can serve for at least 30years.
- To apply our knowledge of civil engineering gained by us in our B.Tech course.


### 1.3.2 ABOUT THE CODE (IRC-103-1988)

Walking is an important mode of transport. Significant trips up to 2 km are on foot and every journey start / end with a walk. Requirements are partly covered in IRC: 70-1977 "Guideline on regulation and control of mixed traffic in urban areas" and IRC: 86-1983 "Geometric design standards for urban roads in plains".

| Width of side walk <br> (meters) | Capacity <br> (Number of persons per hour) |  |
| :---: | :---: | :---: |
| 1.50 | All in one direction | In both the directions |
| 2.00 | 1200 | 800 |
| 2.50 | 2400 | 1600 |
| 3.00 | 3600 | 2400 |
| 4.00 | 4800 | 3200 |
|  | 6000 | 4000 |

Table 1.1 Capacity of side walks

- General Principles:

1. Pedestrian facilities should be planned in an integrated manner to ensure continuous flow.
2. Reduce conflict between pedestrian and vehicles.
3. Convenience is paramount. ${ }^{[3]}$

- Footpath/Sidewalk:

1. Should be on both sides.
2. Minimum Width of 1.5 meters.
3. There are criteria based on pedestrians per hour (as shown in Table1.1)
4. In shopping areas, width should be increased by 1 m (to be treated as dead width).
5. When adjacent to buildings, fences - dead width has to be 0.5 meters. ${ }^{[3]}$

- Guard Rails:

1. Two aspects which need special consideration are:-
a. The height of hand-rail.
b. The obstruction to visibility.
2. The design should be neat, simple in appearance and as far as possible, vandal proof. ${ }^{[3]}$

- Zebra Crossing:

1. Width: -2 to 4 meters.
2. Nit within 150 meters from each other.
3. Median strip should be of adequate width (this is only reference to pedestrian refugee). ${ }^{[3]}$

- What is missing?

1. No mention of right of way for pedestrians at non-signal controlled zebra crossings (though Delhi Police website says so)
2. No mention on height of footpaths.
3. No mention on dipped kerbs and gradients
4. No mention of slip free tilting (needed usually on dipped kerbs).
5. No mention on pedestrian refugee and types
6. Signal phases are mentioned but no guideline on timings.
7. No mention with regards width around street furniture (bus stops, trees, benches, bins, electricity meter boxes, post boxes, signage poles, street lightning).

## CHAPTER-2

## SURVEYING

### 2.1 GENERAL

Surveying is the art of determining the relative position of points on, above or beneath the surface of the earth by means of direct or indirect measurement of distance direction and elevation. It includes the art of establishing points by predetermined angular and linear measurements.

The knowledge of surveying is advantageous in many phases of engineering. The earlier surveys were made in connection with land surveying. Practically every engineering project such as road, water supply and irrigation schemes, railroads and transmission lines, mines, bridges and buildings etc. require surveys. Before plans and estimates are prepared, boundaries should be determined and the topography of the site should be ascertained. After the plans are made, the structure must be staked out in the ground. As the work progresses, lines and grades must be given. ${ }^{[3][4]}$

In surveying all measurements of lengths are horizontal, or else are subsequently reduced horizontal distances. The object of a survey is to prepare plan or map so that it may represents the area on a horizontal plane. A plan or map is horizontal projection of an area and shows only horizontal distances of points. ${ }^{[1][7]}$

In this project, we have performed two types of survey:-

1. Photographic Survey
2. Total Station Survey

### 2.2 PHOTOGRAPHIC SURVEY

It is the basic kind of survey in which the surveyor visits the area to be surveyed, takes the photograph of the area under consideration to get idea of the topography, surroundings which helps the surveyor to plan his survey camp and helps him to choose
the method of surveying. Also, if necessary the surveyor can also talk to the local residents of the area.

In our photographic survey we tried to identify the major problems at Shoghi (as shown in figures). While doing the survey we talked to several residents of Shoghi who told us that there is no proper space for pedestrians to walk along the road neither there are any zebra crossing for the people. Also, there is no parking space for the parking of vehicles and thus the drivers park their vehicles along the side of the road causing the pedestrians to walk on the carriage way which may lead to any kind of accident at any point of time.

The photos of the photographic survey are shown in APPENDIX-A.
From the pictures we deduce that:-

1. There is encroachment by the locals.
2. Parking of vehicles is done along the road.
3. Loading and unloading of the goods and people is done by encroaching the areas which are meant for people to walk upon alongside the road.

According to a survey where no sidewalks are provided, or where sidewalks are in poor repair or have missing sections, the following conditions often result in :-

1. People being forced to walk in the carriage way, resulting in increased pedestrian/motor vehicle collisions. About 8 percent of all pedestrian crashes involve people walking along the road.
2. Without a safe and well-maintained place to walk, people are discouraged and, in extreme cases, prevented from walking. For example, children have a difficult time walking to school and seniors cannot access nearby shops.
3. The absence of sidewalks can eliminate access to all destinations for some people with disabilities. Even short gaps in sidewalk facilities make nearby destinations completely inaccessible to these individuals.
4. Not providing a safe place to walk does not accommodate the needs of people who rely on walking as a mode of travel.

Hence, there is a great need of sidewalk at Shoghi and until it is not provided over there a saying will always be there that " आगे की बजाए पीछे देख के चलना चाहिए।"

### 2.3 TOTAL STATION SURVEY

### 2.3.1 TOTAL STATION

A form of an electronic theodolite combined with an electronic distance measuring device (EDM), the primary function is to measure slope distance, vertical angle, and horizontal angle from a setup point to a foresight point most total stations use a modulated near-infrared light emitting diode which sends a beam from the instrument to a prism.

The prism reflects this beam back to the instrument. The portion of the wavelength that leaves the instrument and returns is assessed and calculated. Distance measurements can be related to this measurement.

The accuracy of a total station is dependent on instrument type. Angle Accuracy (Horizontal or Vertical) can range from 2" to $5 "$. Distance Accuracy can range from: $+/-(0.8+1 \mathrm{ppm} \times \mathrm{D}) \mathrm{mm}$ to $+/-(3+3 \mathrm{ppm} \times \mathrm{D}) \mathrm{mm}$ Where, $\mathrm{D}=$ distance measured. Accuracy is highly dependent on leveling the instrument. Thus two leveling bubbles are provided on the instrument and are referred to the circular level and the plate level. Circular level is located on the tribrack while plate level is on horizontal axis of instrument just below scope of the total station. Sensitivity of Circular Level $=10^{\prime} / 2 \mathrm{~mm}$. Sensitivity of Plate Level $=30^{\prime \prime} / 2 \mathrm{~mm}$.

Although taping and theodolites are used regularly on site - total stations are also used extensively in surveying, civil engineering and construction because they can measure both distances and angles. The appearance of the total station is similar to that of an electronic theodolite, but the difference is that it is combined with a distance measurement component which is fitted into the telescope. Because the instrument combines both angle and distance measurement in the same unit, it is known as an
integrated total station which can measure horizontal and vertical angles as well as slope distances.

### 2.3.2 ADVANTAGES OF TOTAL STATION

1. Relatively quick collection of information.
2. Multiple surveys can be performed at one set-up location.
3. Easy to perform distance and horizontal measurements with simultaneous calculation of project coordinates (Northing, Easting, and Elevations).
4. Layout of construction site quickly and efficiently.
5. Digital design data from CAD programs can be uploaded to data collector.
6. Daily Survey Information can also be quickly downloaded into CAD which eliminates data manipulation time required using conventional survey techniques.

### 2.3.3 DISADVANTAGES OF TOTAL STATION

1. Vertical elevation accuracy is not as accurate as using conventional survey level and rod technique.
2. Horizontal coordinates are calculated on a rectangular grid system. However, the real world should be based on a spheroid and rectangular coordinates must be transformed to geographic coordinates if projects are large scale.
3. As with any computer-based application "Garbage in equals Garbage out". However, in the case of inaccurate construction surveys "Garbage in equals lawsuits and contractors claims for extras."

### 2.3.4 TYPES OF TOTAL STATION SURVEYING

| Slope Staking | Areas |
| :--- | :--- |
| Topographic Surveys | Intersections |
| Construction Project Layout | Point Projections |
| Leveling | Road (Highway ) surveys |
| Resections | Taping from baseline |
| Traverse Surveys and adjustments | Building Face surveys |

TABLE2.1 Types of total station surveying

### 2.3.5 COMPONENTS OF TOTAL STATION



Fig.2.1 Components of Total Station
[䦽"5.1 Basic Key Operation"


Fig.2.2 Basic Key Operations
Menu Pages:-


Fig.2.3 Мепи Pages of Total Station

### 2.3.6 LEVELING OF TOTAL STATION

Leveling the Total station must be accomplished to sufficient accuracy otherwise the instrument will not report results. Before starting leveling the instrument it should be made sure that all the targets can be seen from the station point. After ensuring the leveling process should be started by following steps:-

## 1. Tripod Setup

Tripod legs should be equally spaced. The tripod head should be approximately leveled .also care should be taken that the head should be directly over survey point.


Fig.2.4 Tripod Setup
2. Mount Total station on tripod

Place instrument on Tripod .Secure with centering screw bracing the instrument with the other hand. Don't forget to insert the battery in Total station before leveling.


Fig.2.5 Mounting of Total Station

## 3. Focus on Survey Point

For this, use the optical plummet on the survey point.


Fig.2.6 Focusing of Survey Point
4. Leveling

Adjust the leveling foot screws to center the survey point in the optical plummet reticle. Center the bubble in the circular level by adjusting the tripod legs.


Fig.2.7 Leveling-A

Loosen the horizontal clamp and turn instrument until plate level is level to two of the leveling foot screws. Center the bubble using the leveling screwsthe bubble moves towards the screw that is turned clockwise.


Fig.2.8 Leveling- $B$

Rotate the instrument 90 degrees and level using the third leveling screw.


Fig.2.9 Leveling-C

Observe the survey point in the optical plummet and center the point by loosening the centering screw and sliding the entire instrument. After re-tightening the centering screw check to make sure that the plate level bubble is level in several directions.
5. Electronically Verify Leveling

Turn on the instrument by pressing and holding the "ON" button (you should hear an audible beep).The opening screen will be the "MEAS" screen. Select the [TILT] function. Adjust the foot level screws to exactly center the electronic "bubble". Rotate the instrument $90^{\circ}$ and repeat.


Fig.2.10 Verifying of Leveling
2.3.7 ACCESSORIES OF TOTAL STATION


### 2.3.8 HOW SURVEY WAS DONE AT SHOGHI?

The main aim of doing survey at Shoghi was to prepare a layout of the 1.1 Km long stretch so that we could plan our design of sidewalk accordingly as well as to identify the areas where we have to give the zebra crossings and where we have to leave opening spaces.Through, total station we measured three Distances as shown in the figure namely $\mathrm{D}_{12}, \mathrm{D}_{23}$ and $\mathrm{D}_{34}$.


Fig.2.12 The various distances by total station survey
Where,
$\mathrm{D}_{12}$ - Distance between the left side's outer most point and the left side of the road (black top).
$\mathrm{D}_{23}$ - Width of the carriage way at several cross sections.
$\mathrm{D}_{23}$ - Distance between the right side's outer most point and the right side of the road (black top). ('NOTE- these distances are measured while moving from housing board colony GateNo.2, Shoghi TO 'The Starting of Bye Pass Road to Mehli from Shoghi.

The Data Sheets of the survey are shown in APPENDIX-B.

## CHAPTER-3

## MODELLING

### 3.1 GENERAL

In modeling, we have used the AUTO CAD software to prepare a layout of the 1.1 Km long highway stretch by using the data points which were obtained from the Total Station Survey as discussed in the previous Chapter-2.

Though Auto Cad provides a large number of functions and tools to the users but here to prepare the layout we have used the basic commands such as

1. Drawing Commands: - To draw objects like Line, Poly line, Circle, Hatch etc.
2. Modifying Commands: - To edit the orientation of the objects commands like Copy, Paste, Rotate, Move, Mirror, Trim, Extend and Offset have been used.
3. Other Commands:-
a. LAYERS - These allow the user to assign different line types and colours to named layers. For example, a layer may for red continuous lines, another may be for green hidden lines, and yet another for blue centre lines.
b. UNITS - This command allows the user to set the insertion scale for the drawing and also helps to set the 'Length' and 'Angle' type and precision.
c. DIMALIGNED
d. DIMLINEAR
e. DCLINEAR
f. DCALIGNED
g. MTEXT

### 3.2 PROCEDURE

Here, in Auto Cad we have to prepare the layout using the total survey data points. So here we imported these data points to get the layout by following steps:-

Step1:- Before importing the points and draw the layout we set the units and layers of the lines to be drawn. For this to be done we used 'UNITS' and the 'LAYER' commands. On entering the units command a pop window comes on the screen where we set the insertion units to 'Meters' and angle type to 'Surveyor's Units'.


Fig.3.1 Snapshot-1 from Auto-CAD

After then type the 'LAYER' command and then add new layers of different colors.
For Example:-



Fig.3.3 Snapshot-3 from Auto-CAD

Step2:- Since the drawing conditions are set and the adequate layer is 'on' in Auto CAD. It's time to import. Type the command 'LINE' and then move to the EXCEL SHEET where you have prepared the data points in the required ( $\mathrm{X}, \mathrm{Y}$ ) format.

In the EXCEL Sheet select the points that are falling in one line, copy them and then paste them in the command line of Auto CAD. The Auto CAD will join all the points by making a line between two consecutive points.

Here, we achieved the whole layout by joining drawings made in the same fashion upto each change of station of Total Station. After then hatching was done with solid colour to show the carriage way.

Step3:- After the layout has been made select the different layer to show the cross section lines and then name them using the 'MTEXT' command. Here, to represent the Cross sections we have used the letters "C.S." followed by the corresponding numeral of the cross section. For example, the first cross section which was at the starting point of the survey is represented as C.S. 1 and the last cross section which was at 1090 m is represented as C.S. 78 .

Step4:- As the cross sections have been made and it has been decided that the sidewalk 1.5 m wide will be provided at the left hand side of the carriage way (while moving from H.B. Colony Gate No. 2 to Shoghi Bye Pass Road) and the length of each section of side walk will be 2.0 m which is supported by 3 I-beam girders equidistant from each other. Then, to show the alignment of sidewalk along the stretch we have taken 'OFFSET' of the left hand side of the carriage way line first at $0.20 \mathrm{~m} ; 0.575 \mathrm{~m} ; 0.950 \mathrm{~m} ; 1.325 \mathrm{~m}$; 1.700 m . (Measuring from the left side carriage way line) using a different layer and 'POLYLINE'.

Step5:- After the sidewalk alignment is made, the cross-sections of sidewalk which are at 2.0m apart from each other are made using the 'CIRCLE', 'LINE', 'TRIM' and 'EXTEND' commands of Auto CAD. For this also a separate layer should be used.

Step6:- In this step concrete column placement was find out in two steps:-
a) Drawing of concrete columns of size 0.3 mx 0.3 m at each intersection of sidewalk lines and sidewalk cross section lines by again using the 'OFFSET', 'TRIM', 'EXTEND' commands.
b) Removal of those concrete columns which fall beyond the outermost left side of the carriage way (while moving from H.B. Colony Gate No. 2 to Shoghi Bye Pass Road)using the erase command.

Note:- DIMALIGNED, DIMLINEAR, DCLINEAR, DCALIGNED commands were used to view the aligned and linear distances while drawing the layout.

So, by these six simple steps the modeling from total station data was completed and designing is started all along. (All these steps are shown below in layout diagrams).

Fig.3.4 LINE DIAGRAM OF SHOGHI ROAD OBTAINED FROM TOTALSTATION SURVEY DATA


| S.No. | Line Description | SYMBOL |
| :---: | :--- | :---: |
| 1. | Outter most points at the Left side | LINE-1 |
| 2. | Left side of the road (black top) | LINE-2 |
| 3. | Right side of the road (black top) | LINE-3 |
| 4. | Outter most points at the Right side | LINE-4 |
| Note:- |  |  |
| Moving from 'Housing board colony Gate No.2,Shoghi' <br> 'The Starting of Bye Pass Road to Mehli from Shoghi'). |  |  |

Fig.3.5 LINE DIAGRAM OF SHOGHI ROAD SHOWING CROSS-SECTIONS OF SURVEY DATA


| S.No. | Line Description | SYMBOL |
| :---: | :--- | :---: |
| 1. | Outter most points at the Left side | LINE-1 |
| 2. | Left side of the road (black top) | LINE-2 |
| 3. | Right side of the road (black top) | LINE-3 |
| 4. | Outter most points at the Right side | LINE-4 |
| 5. | Cross-Section Line | LINE-5 |
| Note:-(Moving from 'Housing board colony Gate No.2,Shoghi' <br> TO <br> 'The Starting of Bye Pass Road to Mehli from Shoghi'). |  |  |




## CHAPTER-4

## DESIGNING \& ANALYSIS

### 4.1 GENERAL

In the designing part we decided that we will be doing the designing of the sidewalk in two parts:-

PART I- Providing steel sections from Cross Section No. 1 (Housing Board Colony Gate No.-1) to the Cross section No. 73 (At the junction of village road with the National Highway before the start of Shoghi market).

PART II- Providing concrete sidewalk from Cross Section No. 73 to Cross Section No. 78

### 4.2 DESIGN OF STEEL SIDEWALK:-

Here we have decided to take a section of $2.0 \mathrm{~m} \times 1.5 \mathrm{~m}$ for our sidewalk which will be raised from the earth/road surface at a height of 30 cm fitted with the supports made of concrete columns of initial proposed height 0.5 m and dimensions $0.3 \mathrm{~m} \times 0.3 \mathrm{~m}$. Our main goal is to make the structure light as far as possible without compromising the load carrying capacity of the structure so that the pedestrians can walk upon the sidewalk without any fear and worry of safety.

The section of $2.0 \mathrm{~m} \times 1.5 \mathrm{~m}$ is a simple frame structure (which is differentiated on the basis of supports) consisting of ISA90x90x8 and steel strips of $2 \times 5 \mathrm{~cm}$ as horizontal members, ISJC150 of length 0.3 m are used as columns for the transferring of loads to the concrete supports buried in the soil. Here, we are taking a load of $6 \mathrm{KN} / \mathrm{m}^{2}$ acting on the section along with the self-weight of the members present in the section and for the analysis of the section we are using 'STAAD.Pro V8i' version 2007.


Fig.4.1Loading Conditions

### 4.2.1 TYPES OF STEEL SECTIONS

Based on the support conditions we have classified the section into 16 categories as follows:-

| TYPE No. | STARTING <br> SUPPORT OF <br> CROSS-SECTION | ENDING <br> SUPPORT OF <br> CROSS-SECTION | NUMBER OF <br> CROSS-SECTION <br> ACCORDING TO <br> APPENDIX-C |
| :---: | :---: | :---: | :---: |
| 1. | FIXED | FIXED | 124 |
| 2. | FIXED | P.C.1 | 11 |
| 3. | FIXED | P.C.2 | 2 |
| 4. | FIXED | CANTILEVER | 0 |
| 5. | P.C.1 | FIXED | 10 |
| 6. | P.C.1 | P.C.1 | 26 |
| 7. | P.C. 1 | P.C.2 | 10 |
| 8. | P.C. | CANTILEVER | 1 |


| TYPE No. | STARTING <br> SUPPORT OF <br> CROSS-SECTION | ENDING <br> SUPPORT OF <br> CROSS-SECTION | NUMBER OF <br> CROSS-SECTION <br> ACCORDING TO <br> APPENDIX-C |
| :---: | :---: | :---: | :---: |
| 9. | P.C.2 | FIXED | 1 |
| 10. | P.C.2 | P.C.1 | 12 |
| 11. | P.C.2 | P.C.2 | 53 |
| 12. | P.C.2 | CANTILEVER | 10 |
| 13. | CANTILEVER | FIXED | 0 |
| 14. | CANTILEVER | P.C.1 | 0 |
| 15. | CANTILEVER | P.C.2 | 10 |
| 16. | CANTILEVER | CANTILEVER | 167 |

Table 4.1 Loading Condition Summary
Where,

1. P.C. 1 i.e. Propped Cantilever 1:-

Fixed Support is at 1.125 m from the starting end moving transversely on sidewalk along 1.5 m .
2. P.C. 2 i.e. Propped Cantilever 2:-

Fixed Support is at 0.75 m from the starting end moving transversely on sidewalk along 1.5 m .

Though the designing of these types of sections was easy but it would be very difficult for the manufacturer to create and fix these 16types of sections. So we decided to take only three of the sections and replace the others with them. The sections chosen as models were:-

1. TYPE-1 (FIXED-FIXED) Support Section (124No.)
2. TYPE-11 (P.C.2-P.C.2) Support Section (146No.)
3. TYPE-16 (CANTILEVER-CANTILEVER) Support Section (167No.)

Also we have to provide openings, for example near the Good Luck Restaurant at cross section 26-28, near the road to Primary Health Center at cross section 38-39 and at the road to primary school at cross section 52-53. All these openings are accounted in the following estimate part of report. The Staad-Editor code are given in APPENDIX-D.

In all the models to maintain uniformity we have used the following specifications:-

| S.No. | NAME OF <br> ITEM | DIMENSIONS | LENGTH | MATERIAL | USED IN |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 01. | Concrete <br> Column | 0.3 mx 0.3 m | 0.5 m | Concrete | All the sections accordingly |
| 02. | Horizontal <br> Strips | 0.2 mx 0.5 m | 1.5 m | Steel | All the Sections |
| 03. | ISA 90x90x8 ${ }^{[6]}$ | 90 mmx 90 mmx 8 mm | 1.5 m | Steel | All the Sections |
|  |  |  | 0.81 m |  | Model 2 |
|  |  |  | 2.12 m |  | Model 3 |
| 04. | ISJC150 ${ }^{[6]}$ | $\begin{aligned} & \mathrm{h}=150 \mathrm{~mm} \\ & \mathrm{~b}=55 \mathrm{~mm} \\ & \mathrm{t}_{\mathrm{t}}=6.9 \mathrm{~mm} \\ & \mathrm{t}_{\mathrm{w}}=3.6 \mathrm{~mm} \end{aligned}$ | 0.3 m | Steel | All the Sections |
| 05. | ISA 50x50x5 ${ }^{[6]}$ | 50 mmx 50 mmx 5 mm | 2.0m | Steel | Guard Rail |
|  |  |  | 1.3m |  |  |
| 06. | Steel Bars | 20mm- $\phi$ | 1.0 m | Steel | Guard Rail |

Table 4.2 Specifications Table
4.2.1.1 MODEL-1 (FIXED-FIXED) Support Section (124 No.):-


Fig.4.2Model-1 Showing Dimensions


Fig.4.3 Model-1 showing member properties
4.2.1.2 MODEL-2 (P.C.2-P.C.2) Support Section (146No.):-


Fig.4.4 Model-2 Showing Dimensions


Fig.4.5 Model-2 showing member properties
4.2.1.3 MODEL-3 (CANTILEVER-CANTILEVER) Support Section (167No.):-


Fig.4.6 Model-3 Showing Dimensions


Fig.4.7 Model-3 showing member properties

### 4.2.1.4 GUARD RAIL:-

Pedestrian guard rails are an important design element

1. To prevent indiscriminate crossing and
2. To prevent spilling over of pedestrians on to the carriage way.

The design of guard rails should be neat; simple in appearance and as far as possible should be vandal proof. Two aspects which need special consideration are the height of hand rail and the obstruction to visibility. The visibility of the approaching vehicles by the pedestrians as well as the visibility of the pedestrians by the drivers of the approaching vehicles should be adequate. The guard rails should be sturdy but slender design.

Pedestrian guard rails could normally be considered under the following situations:-
(a) Hazardous locations on straight stretches
(b) At Junctions/Intersections
(c) Schools
(d) Bus Stops, Railway Stations, etc.
(e) Over pass, Subway, etc.
(f) Central reserves.

Provision of Guard-Rails:-



Fig.4.9 Guard Rail-II
Here we'll be providing a section of length $2.0 \mathrm{~m} \times 1.3 \mathrm{~m}$ as shown in Fig.4.8 and Fig.4.9. In the section all the joints are made by welding the members to each other. And the whole sections are joined to each other as shown in Fig4.10.


Fig.4.10 Guard Rail-Joint Section

Other Considerations:-

- There will be no gaps in between the guard rails.
- Also, guard rails will be providing on both the sides of the sidewalk.


### 4.3 DESIGN OF CONCRETE SIDEWALK ${ }^{[6]}$ :-

The concrete sidewalk will be provided from the Cross-Section No. 73 to Cross-Section No. 78 i.e. for the whole market area. Following are the few considerations:-

- Width of the Sidewalk $=2.0 \mathrm{~m}$
- Height of the Sidewalk $=30 \mathrm{~cm}$
- Transverse Slope of the Side Walk $=1: 15$
- Grade of Concrete Used $=$ M20 (1:1.5:3)
- Water/Cement Ratio= 0.5
- Calculation of dry materials:-
- Ratio=1:1.5:3
- Sum $=1+1.5+3=5.5$
- Total dry mortar for $1 \mathrm{~m}^{3}$ of cement concrete $=1.20 \mathrm{~m}^{3}$
(Considering a wastage of 20\%)
- Therefore the materials required for $1 \mathrm{~m}^{3}$ of cement concrete are:-
- $\quad$ Cement $=\frac{\mathbf{1 * 1 . 2 0 * 2 8 . 8}}{\mathbf{5 . 5}}=6.284$ bags
- $\quad$ Sand $=\frac{2.65 * 1.20}{5.5}=0.578 \mathrm{~m}^{3}$
- Aggregates $=\frac{\mathbf{2 . 8} * \mathbf{1 . 2 0}}{5.5}=0.611 \mathrm{~m}^{3}$
- Volume of Water for $1 \mathrm{~m}^{3}$ of Concrete $=\frac{6.284 \times 0.5 \times 50}{1000}=0.1571 \mathrm{~m}^{3}$


Fig.4.11 Transverse Section of the concrete sidewalk

- Determination of Length of Sidewalk covered with $1 \mathrm{~m}^{3}$ of concrete:-
- Area of Cross-Section as shown in Fig.4.11 $=\frac{\mathbf{1}}{\mathbf{2}} \mathrm{x}(0.3+0.4) \times 1.5=\mathbf{0 . 5 2 5} \mathbf{m}^{\mathbf{2}}$
- $0.525 \mathrm{~m}^{2} \mathrm{x}$ (Length of Sidewalk) $=1 \mathrm{~m}^{3}$
$\Longrightarrow$ Length of Sidewalk $=\frac{1}{0.525}=1.905 \mathrm{~m}$
- Total volume of concrete required for sidewalk of width 1.5 m and length 150 m

$$
=\frac{150}{1.905} \mathrm{~m}^{3}=78.74 \mathrm{~m}^{3}
$$

- Also concrete required to make the supports columns ( 656 No .) of length 0.5 m and dimensions $0.3 \mathrm{mx} 0.3 \mathrm{~m}=656 \times 0.3 \times 0.3 \times 0.5=\mathbf{2 9 . 5 2} \mathbf{m}^{\mathbf{3}}$
- So net volume of concrete required $=29.52+78.74=\mathbf{1 0 8 . 2 6} \mathbf{~ m}^{\mathbf{3}}$


### 4.4 CALCULATION OF LENGTH OF WELD ${ }^{[5]}$

We calculated the length of Weld using the MACROS feature of MS-Excel in which we used as follows:-

Sub WELDED()
'Enter data
$\mathrm{fu}=\operatorname{Cells}(3,5)$
$\mathrm{fy}=\operatorname{Cells}(4,5)$
$\mathrm{Gmw}=\operatorname{Cells}(5,5)$
'thickness of plate t '
$\mathrm{t}=\operatorname{Cells}(6,5)$
'Angle of Weld A'
$\mathrm{A}=\operatorname{Cells}(7,5)$
'Force to be handled F'
$\mathrm{F}=\operatorname{Cells}(8,5)$

Smin $=0$
'Size of Weld,S'
If $0<t$ And $t<=10$ Then

$$
\operatorname{Smin}=3
$$

ElseIf $11<\mathrm{t}$ And $\mathrm{t}<=20$ Then

$$
\operatorname{Smin}=5
$$

ElseIf $21<\mathrm{t}$ And $\mathrm{t}<=32$ Then
Smin $=6$
ElseIf $33<\mathrm{t}$ And $\mathrm{t}<=50$ Then
Smin $=8$
GoTo Skip1
End If

Skip1:
$\operatorname{Cells}(10,5)=\operatorname{Smin}$
$\mathrm{TT}=0$
'Throat thickness TT'
If $60<=$ A And A <= 90 Then $\mathrm{TT}=0.7$ * Smin

ElseIf $91<=$ A And A <= 100 Then

$$
\mathrm{TT}=0.65 * \operatorname{Smin}
$$

ElseIf $101<=$ A And A <= 106 Then $\mathrm{TT}=0.6 * \operatorname{Smin}$

ElseIf $107<=$ A And A <= 113 Then $\mathrm{TT}=0.55 * \operatorname{Smin}$

ElseIf $114<=$ A And A <= 120 Then $\mathrm{TT}=0.5 * \operatorname{Smin}$

Else
GoTo Skip2
End If

Skip2:
$\operatorname{Cells}(11,5)=\mathrm{TT}$
'Length of Weld L'
$\mathrm{L}=\left(\mathrm{F} *\left((3)^{\wedge} 0.5\right) * \mathrm{Gmw}\right) /(\mathrm{fu} * \mathrm{TT})$
$\operatorname{Cells}(13,5)=\mathrm{L}$
'Total Length of Weld'
$\mathrm{TL}=\mathrm{L}+(2$ * Smin$)$
$\operatorname{Cells}(14,5)=\mathrm{TL}$

End SubExample data is shown in Table 4.3


| 7 | Minimum Size of <br> Weld | S | $=$ | 3 |
| :---: | :--- | :--- | :--- | :--- |
| mm |  |  |  |  |
| 8 | Throat Thickness | T | $=$ | 2.1 |
| mm |  |  |  |  |


| 9 | Length of Weld | L | $=18.5$ | mm |
| :---: | :--- | :---: | :---: | ---: | :--- |
| 10 | Total Length of Weld | L+2S | $=24.5$ | mm |

Table 4.3 Length of Weld for Model-1

### 4.5 CALCULATION OF DEVELOPMENT LENGTH ${ }^{[4][5]}$

We calculated the length of Weld using the MACROS feature of MS-Excel in which we used as follows:-

Sub DevelopmentLength()
'Enter Data
'Area of Cross Section,A
$\mathrm{A}=\operatorname{Cells}(3,5)$
'perimeter of Cross Section,p
$\mathrm{P}=\operatorname{Cells}(4,5)$
$\mathrm{fvd}=\operatorname{Cells}(5,5)$

If Cells(6, 5) $=$ "YES" And Cells(7, 5) $=$ "M10" Then

$$
\mathrm{Tbd}=1.2
$$

Else

## GoTo Skip0

End If

## Skip0:

If Cells(6, 5) = "YES" And Cells(7, 5) = "M20" Then

$$
\operatorname{Tbd}=1.2+(0.2 * 1.2)
$$

Else

GoTo Skip1

End If

Skip1:

If Cells(6, 5) = "YES" And Cells(7, 5) = "M25" Then

$$
\operatorname{Tbd}=1.4+(0.2 * 1.4)
$$

Else

## GoTo Skip2

End If

Skip2:
If Cells(6, 5) = "YES" And Cells(7, 5) = "M30" Then

$$
\operatorname{Tbd}=1.5+(0.2 * 1.5)
$$

Else

## GoTo Skip3

End If

## Skip3:

If Cells(6, 5) = "YES" And Cells(7, 5) = "M35" Then

$$
\mathrm{Tbd}=1.7+(0.2 * 1.7)
$$

Else

GoTo Skip4

End If

Skip4:

If Cells(6, 5) = "YES" And Cells(7, 5) = "M40" Then

$$
\operatorname{Tbd}=1.9+(0.2 * 1.9)
$$

Else

## GoTo Skip5

End If

Skip5:
If Cells $(6,5)=$ "NO" And Cells $(7,5)=$ "M20" Then $\mathrm{Tbd}=1.2$

Else

GoTo Skip6

End If

Skip6:

If Cells $(6,5)=$ "NO" And Cells $(7,5)=$ "M25" Then
$\mathrm{Tbd}=1.4$

Else

## GoTo Skip7

End If

## Skip7:

If Cells $(6,5)=$ "NO" And Cells(7, 5) $=$ "M30" Then $\mathrm{Tbd}=1.5$

Else

GoTo Skip8

End If

Skip8:

If Cells $(6,5)=$ "NO" And Cells(7, 5) $=$ "M35" Then
$\mathrm{Tbd}=1.7$

Else

## GoTo Skip9

End If

Skip9:

If Cells $(6,5)=$ "NO" And Cells(7,5) $=$ "M40" Then
$\mathrm{Tbd}=1.9$

End If
$\operatorname{Cells}(8,5)=\operatorname{Tbd}$
'Development Length,Ld
$\mathrm{Ld}=(\mathrm{A} * \mathrm{fvd}) /(\mathrm{Tbd} * \mathrm{P})$
$\operatorname{Cells}(10,5)=\operatorname{Ld}$
'Force in the Member,F
$\mathrm{F}=\operatorname{Cells}(12,5)$
'Required Development Length,RLd
$\operatorname{RLd}=(\mathrm{A} * \mathrm{~F}) /(\mathrm{Tbd} * \mathrm{P})$
$\operatorname{Cells}(13,5)=\operatorname{RLd}$

End Sub

Example data is shown in Table 4.4

| S.No. | ENTITY | SYMBOLS | VALUES | UNITS |  |  |
| :---: | :--- | :---: | :--- | :--- | :--- | :---: |
|  |  |  |  |  |  |  |
| 1 | Area of Cross Section | A | $=$ | 1265 | $\mathrm{~mm}^{2}$ |  |
| 2 | Perimeter of Cross Section | P | $=$ | 512.8 | mm |  |
| 3 | $\mathrm{f}_{\mathrm{vd}}$ |  | $=$ | 250 | $\mathrm{~N} / \mathrm{mm}^{2}$ |  |
| 4 | Whether it is a compression member? |  | $=$ | YES |  |  |
| 5 | Grade of concrete |  | $=$ | M 20 |  |  |
| 6 | $\tau_{\text {bd }}{ }^{[4]}$ |  | $=$ | 1.44 | $\mathrm{~N} / \mathrm{mm}^{2}$ |  |


| 7 | Maximum Development Length | $\mathrm{L}_{\mathrm{d}}$ | $=428.27$ | mm |
| :--- | :--- | :--- | :--- | :--- |


| 8 | Stress in the member | F | $=45.404$ | $\mathrm{~N} / \mathrm{mm}^{2}$ |
| :---: | :--- | :---: | :---: | :--- |
| 9 | Required Development Length | $\mathrm{L}_{\mathrm{d}}$ required | $=77.8$ | mm |

Table 4.4 Development Length for Model-1

## CHAPTER-5

## ESTIMATION \& COSTING

### 5.1 GENERAL

In this chapter we have done quantity estimation and based on that we have calculated the cost for the whole project using the 'Standard Schedule of Rates 2009 - HIMACHAL PRADESH PUBLIC WORKS DEPARTMENT (Building Civil Works)'.

### 5.2 ESTIMATE OF QUANTITIES

| Detail of Measurements |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Name of Work- Proposed Sidewalk along the Ambala-Shimla National Highway-5 at Shoghi , Himachal Pradesh of Length 1.1 Km . |  |  |  |  |  |  |  |  |
| S.No. | Description of Items | Nos. |  | $\begin{gathered} \mathbf{L} \\ (\mathbf{m}) \end{gathered}$ | $\underset{(\mathbf{m})}{\text { B }}$ | $\begin{gathered} \mathbf{H} / \mathbf{D} \\ (\mathbf{m}) \end{gathered}$ | QTY. <br> (m) | REMARKS |
|  |  | SEC. | SIDE |  |  |  |  |  |


| 1 | AMOUNT OF STEEL IN <br> WELDED BUILT-UP <br> SECTIONS FOR STEEL SIDE <br> WALK |
| :---: | :--- |


| (a) | MODEL 1 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (i) | ST ISJC150 | 122 | 1.2 | 146.4 | Rmt. | $122 * 1.2$ |
| (ii) | ST ISA90*90*8 | 122 | 7 | 854 | " | 122 * 7 |
| (iii) | $\begin{aligned} & \text { PRISMATIC STEEL } \\ & \text { (39strips per section) } \\ & (0.03 \times 0.03 \mathrm{~m}) \end{aligned}$ | 122 | 58.5 | 7137 | " | $122 * 58.5$ |



| S.No. | Description of Items | Nos. |  | $\begin{gathered} \mathbf{L} \\ (\mathbf{m}) \end{gathered}$ | $\begin{gathered} \text { B } \\ (\mathbf{m}) \end{gathered}$ | $\begin{gathered} \mathbf{H} / \mathbf{D} \\ (\mathbf{m}) \end{gathered}$ | QTY. <br> (m) | REMARKS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | SEC. | SIDE |  |  |  |  |  |


| (c) | MODEL 3 |  |  |  |  |  |  |  |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (i) | ST ISJC150 | 155 |  | 0.6 |  |  | 93 | $"$ | $155 * 0.6$ |
| (ii) | ST ISA90*90*8 | 155 |  | 11.24 |  |  | 1742.2 | $"$ | $155 * 11.24$ |
| (iii) | PRISMATIC STEEL <br> $(39$ strips per section) <br> $(0.03 \times 0.03 \mathrm{~m})$ | 155 |  | 58.5 |  |  | 9067.5 | " | $155 * 58.5$ |


| (d) | GUARD RAIL |  |  |  |  |  |  |  |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (i) | ST ISA50*50*5 | 810 |  | 6.6 |  |  | 5346 | $"$ | $810 * 6.6$ |
| (ii) | Steel bar of 20 mm dia | 810 |  | 19 |  |  | 15390 | $"$ | $810 * 19$ |




| S.No. | Description of Items | Nos. |  | $\begin{gathered} \mathbf{L} \\ (\mathbf{m}) \end{gathered}$ | $\begin{gathered} \mathbf{B} \\ (\mathbf{m}) \end{gathered}$ | $\begin{gathered} \text { H/D } \\ (\mathbf{m}) \end{gathered}$ | QTY. <br> (m) |  | REMARKS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | SEC. | SIDE |  |  |  |  |  |  |
|  | Between the strips \& the angle | 6045 | 2 | 0.0269 |  |  | 325.221 | ' | $\begin{gathered} \hline 39 * 155 * 2 * \\ 0.0269 \\ \hline \end{gathered}$ |
|  | Between the slant angle \& horizontal angle | 155 | 2 | 0.0269 |  |  | 8.339 | " | $\begin{aligned} & 155 * 2 * \\ & 0.0269 \end{aligned}$ |
| (iv) Guard rail |  |  |  |  |  |  |  |  |  |
|  | 20mm dia bars connected to ISA50*50*8 | 19 | 2 | 0.1256 |  |  | 4.773 | " | $19 * 2 * 0.1256$ |


| (g) | NUMBER OF BOLTS <br> (MS20mm DIA) USED IN <br> GUARD RAIL <br> CONNECTIONS | 810 | 1 |  |  |  | 810 | No. |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| NET QUANTITY ESTIMATE FOR STEEL SIDEWALK |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Description of Items | Nos. |  | QTY. |  | WT./ MTR. <br> (Kg/ <br> Rmt.) | $\begin{aligned} & \text { NET } \\ & \text { QTY. } \end{aligned}$ |  | REMARKS |
| S.No. |  | SECT. | SIDE |  |  |  |  |  |  |
| 1 | ST ISJC150 | 405 |  | 393 | Rmt. | 9.9 | 3891 | Kg | 393*9.9 |
| 2 | ST ISA90*90*8 | 405 |  | 3699.56 | Rmt. | 10.8 | 39955 | Kg | $\begin{aligned} & \hline 3699.568^{*} \\ & 10.8 \end{aligned}$ |
| 3 | PRISMATIC STEEL (39strips per section) ( $0.03 \times 0.03 \mathrm{~m}$ ) | 405 |  | 23692.5 | Rmt. | 7.065 | 167388 | Kg | $\begin{aligned} & 23692.4^{*} \\ & 7.065 \end{aligned}$ |
| 4 | ST ISA50*50*5 | 810 |  | 5346 | Rmt. | 3.8 | 20314.8 | Kg | $\begin{aligned} & \hline 5346^{*} \\ & 3.8 \end{aligned}$ |
| 5 | Steel bar of 20 mm dia | 810 |  | 15390 | Rmt. | 2.47 | 38013.3 | Kg | 15390*2.47 |
| 6 | Welding Rods (No.) 45 cm long \& 4mm thick |  |  | 950.5224 | Rmt. |  | 2112 | RODS | $\begin{aligned} & \hline 1156.41 / \\ & 0.45 \end{aligned}$ |
| 7 | MS 20mm-dia Bolts | 810 |  | 810 | No. |  | 810 | No. |  |

Table 5.1 Quantity estimate for steel section sidewalk

Earlier in Chapter-4 we calculated that $1 \mathrm{~m}^{3}$ of concrete can be used for 1.905 m length of sidewalk and whole length will require a total volume of $78.74 \mathrm{~m}^{3}$ and steel section requires $29.52 \mathrm{~m}^{3}$ of concrete of Grade M20.So, the required weight of concrete's constituents are shown in Table5.2

| NET QUANTITY ESTIMATE FOR CONCRETE SIDEWALK |  |  |  |  |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: |
| S.No. | Description of Items | $\begin{array}{c}\text { QTY. USED } \\ \text { PER } \mathbf{~}^{3} \\ \text { OF }\end{array}$ | $\begin{array}{c}\text { NET QTY. } \\ \text { For } \\ \text { CO8.26m }\end{array}$ | of | REMARKS |
| Concrete |  |  |  |  |  |$]$

Table 5.2 Quantity estimate for concrete section sidewalk

### 5.3 ESTIMATE OF COST

| ABSTRACT OF COST $^{[10]}$ |  |  |  |  |  |
| :---: | :--- | :---: | :---: | :---: | :---: |
| Name of Work- Proposed Sidewalk along the Ambala-Shimla National Highway-5 at <br> Shoghi , Himachal Pradesh of Length 1.1 Km. |  |  |  |  |  |
| S.No. | PARTICULARS | Quantity | Unit | Rate | Amount <br> (Rs.) |
| 1 | ST IS JC150 | 3891 | Kg | Rs.43/Kg | 167313 |
| 2 | ST ISA90*90*8 | 39955 | Kg | Rs.43/Kg | 1718065 |
| 3 | Prismatic Steel (0.03mx0.03m) | 167388 | Kg | Rs.43/Kg | 7197684 |
| 4 | ST ISA50*50*5 | 20314.8 | Kg | Rs.43/Kg | 873536.4 |
| 5 | Steel Bar of 20mm dia. | 38013.3 | Kg | Rs.43/Kg | 1634572 |
| 6 | Welding Rod(45 cm long and 4 mm <br> thick) | 2112 | Rods | Rs5/rod | 10560 |
| 7 | MS 20mm-dia Bolts | 810 | Bolts | Rs45/10Bolts | 3645 |
| 8 | Cement Bags | 680 | $\mathrm{Bags}^{\text {Rs.310/Bag }}$ | 210800 |  |
| 9 | Coarse Aggregates | 63 | $\mathrm{~m}^{3}$ | Rs.581/m ${ }^{3}$ | 30793 |
| 10 | Fine Aggregates | 66 | $\mathrm{~m}^{3}$ | Rs.300/m ${ }^{3}$ | 19800 |
| 11 | Water | 17 | $\mathrm{~m}^{3}$ | $1.5 \%$ to $2 \%$ <br> of total cost <br> of concrete | 5227.86 |
|  |  |  |  |  |  |


| S.No. | PARTICULARS | Quantity | Unit | Rate | Amount <br> (Rs.) |
| :---: | :---: | :---: | :---: | :---: | :---: |


| 12 | Contractor's Profit | TOTAL | 11871996 |
| :---: | :---: | :---: | :---: |

Cost of the project =One Crore Thirty Lacs Fifty Nine Thousand One Hundred Ninety Six Rupees only.

Table 5.3 Abstract of Cost

## CHAPTER-6

## PROPOSED AMMENDEMENTS

### 6.1 PROVISION FOR ZEBRA CROSSINGS AT SHOGHI ${ }^{[3]}$

We are proposing two zebra crossings at the Shoghi highway. It will be provided at the major points where there is an immense need for the pedestrian to cross the road.

- LOCATION OF ZEBRA CROSSINGS
- Near the housing board colony gate no 2 (between cross section 50-51)
- Main market along the bus stand.(between cross section 74-75)
- WIDTH OF ZEBRA CROSSINGS
- Near the housing board colony gate no 2 (between cross section 50-51) 2 m
- Main market along the bus stand.(between cross section 74-75) 3.5 m
- WIDTH OF BLACK AND WHITE STRIPS IN ZEBRA CROSSINGS
- $30-50 \mathrm{~cm}$


Fig.6.1 Zebra-Crossing near the housing board colony at Gate No. 2 (between cross section 50-51)


Fig.6.2 Zebra-Crossing at the main market (between cross section 74-75)

### 6.2 PROVISION FOR SPEED-BREAKERS AT SHOGHI ${ }^{[2]}$

- LOCATION OF SPEED-BREAKERS:-
- The curve where visibility is less (Between cross section 30-31).
- 50 m before the zebra crossing i.e. near the housing board colony gate no. 2 (Between cross-sections 45-46).
- 50m after zebra crossing (At cross-section 56).
- 100m away from bus stand (Between cross-sections 76-77).


Fig.6.3 Speed-Breaker near the curve where sight distance is not visible


Fig.6.4 Speed-Breaker at 50m before the zebra crossing, near the housing board colony gate no. 2 (Between cross-section45-46)


Fig.6.5 Speed Breaker at 50 m after zebra crossing (At cross-section 56)


Fig.6.6 Speed-Breaker at 100m away from bus stand
(Between Cross-Section 76-77)

- DESIGN OF SPEED BREAKERS:-
- Speed breakers are formed basically by providing around it (of 17 m radius) hump of 3.7 m width and 10 cm height for the preferred crossing speed of $25 \mathrm{~km} / \mathrm{h}$ for general traffic.
- To facilitate appreciable and comfortable passage for larger and heavier vehicle humps may be modified with 1.5 m long ramps ( $1: 20$ ) at each edge.
- The distance between one hump to another can vary from (100-120) m centre to centre.


Fig.6.7 Longitudinal Cross-Section of Speed-Breaker

### 6.3 PROVISION FOR SIGN POST AND MARKINGS ${ }^{[2]}$

- DRIVERS SHOULD BE WARNED OF THE presence of speed breakers by posting suitable advanced warning signs. The sign should have definition plate with the words 'SPEED BREAKER' and should be located 40m in advance of the first speed breaker.
- Speed breakers should be painted with alternate black and white bands.

Embedded cat-eyes can also be used to enhance night visibility.

## - SIGN DETAILS:-

- Lateral Placement Left :-
- 0.60 m on kerbed roads.
- 2.3 m on unkerbed roads.
- Mounting Height :-
- 2.0 m on kerbed roads.
- 1.5 m on unkerbed roads.
- Use reflective paint or strip.
- Side of triangle- 60 cm or 90 cm (standard).
- Red Strip width- 4.5 cm or 7.0 cm .
- Post Height- $8 \mathrm{~cm} \times 8 \mathrm{~cm} \times 0.8 \mathrm{~cm}$.
- T-Iron to be painted white and black in alternate 25 cm bands.


Fig.6.8 Sign Post

## CHAPTER-7

## RESULTS AND DISCUSSIONS

### 7.1 RESULTS

- From the Total-Station survey the whole stretch of 1.1 Km was divided into a total number of 78 cross-sections of length $10 \mathrm{~m}, 20 \mathrm{~m}$ and 50 m respectively. Also, the data points were obtained in $(\mathrm{x}, \mathrm{y})$ format for the layout formation from the totalstation survey.
- After preparing the layout in AUTO-CAD, 16 support based models were identified and total number of 437 sections of dimensions $2.0 \mathrm{~m} \times 1.5 \mathrm{~m}$ were classified under these support based models.( up to Cross-Section No.-73).
- A maximum load intensity of $6 \mathrm{KN} / \mathrm{m}^{2}$ was chosen and to make the design as simple as possible, the 16 support based models were incorporated into 3 support based model namely,
- MODEL-1 (FIXED-FIXED) Support Section (124 No.)
- MODEL-2 (P.C.2-P.C.2) Support Section (146 No.)
- MODEL-3 (CANTILEVER-CANTILEVER) Support Section (167 No.) which were analyzed for feasibility on Staad.Pro and MS-Excel (Macros).
- The total estimated quantity cost after considering the openings in the side walk for the project came out to be Rs. One Crore Thirty Lacs Fifty Nine Thousand One Hundred Ninety Six Rupees only. Of which $55.11 \%$ of the total cost is due to the prismatic steel sections of dimensions $(0.03 \mathrm{~cm} \times 0.03 \mathrm{~cm})$ which are 39 in number per section.
- To provide additional safety features for pedestrian recommendations were provided for zebra-crossing and speed breakers. A total of 2 zebra-crossings and 4 speed-breakers are proposed in the report.


### 7.2 DISCUSSIONS

The layout obtained from the data points is similar to the 'Google-Earth' maps. So we can say that our obtained layout is correct.

For designing and analysis of the sidewalk a load of $6 \mathrm{KN} / \mathrm{m}^{2}$ was taken which was more than the specified maximum load in IS $875: 1987$ (Part-2) i.e. $5 \mathrm{KN} / \mathrm{m}^{2}$. It was taken $6 \mathrm{KN} / \mathrm{m}^{2}$ in order to accumulate the load from the pedestrians and for the static load coming from guard rail along with the dynamic load (minor) caused due to the movement of vehicles near the guard rails.

Also the high cost of the project is due to prime condition for maintaining a simple, uniform design. For fulfillment of this condition we have to use heavy sections like ISA90x90x8 and ISJC150 along with prismatic steels members of dimensions 1.5 mx 0.03 mx 0.03 m and if observed carefully about $55.11 \%$ of the cost of the project is due to the prismatic steel member.

But had we used a smaller section as prismatic steel member, all sections were failing under the condition of 'Slenderness Ratio' when the design was checked in reference to IS 800:2007 (for Limit State Design). A steel section rather than 0.03 mx 0.03 m which was not failing under this criteria was 0.02 mx 0.05 m which was adding an additional cost of Rs.28,50,335/- (Rupees Twenty eight lac fifty thousand three hundred thirty five only). So we can say that our designed sidewalk can safely bear a load of $6 \mathrm{KN} / \mathrm{m}^{2}$ and is safe according to the checks of IS 800:2007.

## CONCLUSIONS

At the end of this project report we would like to conclude that our designed steel and concrete sidewalk will be able to bear a live load of $6\left(\mathrm{KN} / \mathrm{m}^{2}\right)$ safely and efficiently without needing any maintenance atleast for the next 20-25 years. We have designed the sidewalk keeping the future perspective in our mind i.e. population increase, increasing locality, schools, hospitals etc as Shoghi is expanding by leaps and bounds.

Also, after surveying the total stretch of 1.1 Km we found that there was not enough space for lying of concrete throughout the stretch. It was only the market place where the concrete sidewalk can be used as by using steel sidewalk we not only increased the cost for the project but also the noise pollution for the area. So we switched for our use of steel sections for the remaining 810 m . Though this increased the cost of the project but to have a safe, efficient, uniform and according to code design it was the price we had to pay.

Thus, we would like to conclude that we were able to fulfill our objectives except for giving an economical design but this project taught us a lot. We not only used our knowledge of subjects like surveying, design of steel structures and concrete technology but also helped us to explore more about these subjects and softwares being used in civil engineering like AutoCAD, Staad.Pro , Tekla Structures etc.

## FUTURE SCOPE OF WORK

Though much work cannot be done in the surveying and modeling part of the project but there is a scope for doing future work in the design optimization of this project.

Rather than using grating of prismatic steel, the girder and thin chequered plate can be used so as to optimize the cost of the project as our design had $55.11 \%$ of total cost of the project because of the use of prismatic steel members. Also one could work on the possibility for making a sidewalk wholly of concrete and reduce the cost to its minimal level.

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## APPENDIX-A

## PHOTOGRAPHIC SURVEY



FigA. 1 Pedestrian walking along the road


Fig.A. 2 Children walking towards school


Fig.A. 3 Bus moving closely to the unpaved shoulder


Fig.A. 4 Motorcycles parked on the road


Fig.A. 5 Encroachment by the shopkeepers on the carriage way


Fig.A. 6 Loading and unloading on the carriage way


Fig.A. 7 Repair work of vehicles on the along the road


Fig.A. 8 Open drainage along the road


Fig.A. 9 Snapshot of bus station


Fig.A. 10 No space to walk for the pedestrian


FigA. 11 Snapshot of open drainage


Fig.A. 12 traffic jam at Shoghi bypass


Fig.A. 13 Vehicles parked along the road

## APPENDIX-B

## TOTAL STATION SURVEY DATA AND CALCULATED DISTANCES

| $\begin{gathered} \text { CROSS } \\ \text { SECTION } \end{gathered}$ | Distance from previous C.S. | POINT | N | E | Z | $\begin{aligned} & \text { D12 } \\ & \text { (cm) } \end{aligned}$ | $\begin{gathered} \text { D23 } \\ \text { (m) } \end{gathered}$ | $\begin{aligned} & \text { D34 } \\ & (\mathrm{cm}) \end{aligned}$ | REMARKS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C.S. 1 | 0 | A1 | -0.672 | -1.588 | 0.132 | 278.0 | 6.725 | 174.0 |  |
|  |  | A2 | 0.459 | 0.952 | 0.003 |  |  |  |  |
|  |  | A3 | 3.039 | 7.162 | 0.035 |  |  |  |  |
|  |  | A4 | 3.755 | 8.748 | 0.092 |  |  |  |  |
| C.S. 2 | 10 | B1 | 8.171 | -6.46 | 0.255 | 310.7 | 7.045 | 319.3 |  |
|  |  | B2 | 9.426 | -3.618 | 0.072 |  |  |  |  |
|  |  | B3 | 12.55 | 2.696 | 0.019 |  |  |  |  |
|  |  | B4 | 14.123 | 5.475 | 0.041 |  |  |  |  |
| C.S. 3 | 20 | C1 | 17.241 | -10.263 | 0.298 | 248.8 | 7.149 | 393.3 |  |
|  |  | C2 | 18.254 | -7.991 | 0.202 |  |  |  |  |
|  |  | C3 | 21.183 | -1.47 | 0.123 |  |  |  |  |
|  |  | C4 | 22.908 | 2.065 | 0.088 |  |  |  |  |
| C.S. 4 | 30 | D1 | 26.562 | -13.565 | 0.22 | 100.5 | 7.405 | 332.1 |  |
|  |  | D2 | 27.063 | -12.694 | 0.251 |  |  |  |  |
|  |  | D3 | 29.974 | -5.885 | 0.21 |  |  |  |  |
|  |  | D4 | 31.683 | -3.038 | 0.222 |  |  |  |  |
| C.S. 5 | 40 | E1 | 35.299 | -18.214 | 0.281 | 80.8 | 7.617 | 292.3 |  |
|  |  | E2 | 35.732 | -17.532 | 0.283 |  |  |  |  |
|  |  | E3 | 38.798 | -10.559 | 0.353 |  |  |  |  |
|  |  | E4 | 40.182 | -7.984 | 0.356 |  |  |  |  |
| C.S. 6 | 50 | F1 | 43.726 | -23.298 | 0.554 | 85.3 | 7.405 | 295.1 |  |
|  |  | F2 | 44.217 | -22.6 | 0.383 |  |  |  |  |
|  |  | F3 | 47.164 | -15.807 | 0.604 |  |  |  |  |
|  |  | F4 | 48.618 | -13.239 | 0.365 |  |  |  |  |
| C.S. 7 | 60 | G1 | 49.921 | -30.441 | 0.636 | 251.5 | 7.604 | 406.7 |  |
|  |  | G2 | 51.864 | -28.844 | 0.532 |  |  |  |  |
|  |  | G3 | 55.01 | -21.921 | 0.832 |  |  |  |  |
|  |  | G4 | 57.529 | -18.728 | 0.718 |  |  |  |  |


| $\begin{aligned} & \text { CROSS } \\ & \text { SECTION } \end{aligned}$ | Distance from previous C.S. | POINT | N | E | Z | $\begin{aligned} & \text { D12 } \\ & (\mathrm{cm}) \end{aligned}$ | $\begin{gathered} \text { D23 } \\ \text { (m) } \end{gathered}$ | $\begin{aligned} & \text { D34 } \\ & \text { (cm) } \end{aligned}$ | REMARKS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C.S. 8 | 70 | H1 | 61.225 | -31.542 | 0.695 | 308.9 | 8.284 | 471.8 |  |
|  |  | H2 | 61.951 | -28.54 | 0.745 |  |  |  |  |
|  |  | H3 | 60.159 | -20.452 | 0.942 |  |  |  |  |
|  |  | H4 | 61.5 | -15.929 | 0.804 |  |  |  |  |
| C.S. 9 | 80 | I1 | 71.166 | -33.453 | 0.914 | 276.6 | 8.524 | 270.2 |  |
|  |  | I2 | 71.711 | -30.741 | 1.028 |  |  |  |  |
|  |  | I3 | 70.047 | -22.381 | 0.928 |  |  |  |  |
|  |  | I4 | 70.835 | -19.796 | 0.895 |  |  |  |  |
| C.S. 10 | 90 | J1 | 81.092 | -35.358 | 1.292 | 270.7 | 8.570 | 164.5 |  |
|  |  | J2 | 81.362 | -32.664 | 1.5 |  |  |  |  |
|  |  | J3 | 79.774 | -24.242 | 1.09 |  |  |  |  |
|  |  | J4 | 80.105 | -22.631 | 0.891 |  |  |  |  |
| C.S. 11 | 100 | K1 | 91.145 | -37.24 | 1.678 | 315.2 | 8.309 | 114.7 |  |
|  |  | K2 | 91.312 | -34.092 | 1.872 |  |  |  |  |
|  |  | K3 | 89.62 | -25.957 | 1.36 |  |  |  |  |
|  |  | K4 | 89.66 | -24.811 | 1.305 |  |  |  |  |
| C.S. 12 | 110 | L1 | 101.317 | -36.598 | 2.086 | 322.4 | 8.133 | 103.9 |  |
|  |  | L2 | 101.288 | -33.374 | 2.157 |  |  |  |  |
|  |  | L3 | 99.572 | -25.424 | 1.568 |  |  |  |  |
|  |  | L4 | 99.538 | -24.386 | 1.47 |  |  |  |  |
| C.S. 13 | 120 | M1 | 106.23 | -25.705 | 2.499 | 187.6 | 8.174 | 151.5 |  |
|  |  | M2 | 104.404 | -25.276 | 2.331 |  |  |  |  |
|  |  | M3 | 96.904 | -22.026 | 1.727 |  |  |  |  |
|  |  | M4 | 95.453 | -21.591 | 1.617 |  |  |  |  |
| C.S. 14 | 130 | N1 | 108.522 | -15.853 | 2.515 | 197.0 | 8.631 | 188.7 |  |
|  |  | N2 | 106.567 | -15.607 | 2.45 |  |  |  |  |
|  |  | N3 | 98.634 | -12.208 | 1.919 |  |  |  |  |
|  |  | N4 | 96.776 | -11.877 | 1.741 |  |  |  |  |
| C.S. 15 | 140 | O1 | 110.099 | -5.561 | 2.697 | 283.2 | 8.928 | 171.6 |  |
|  |  | O2 | 107.267 | $-5.564$ | 2.593 |  |  |  |  |
|  |  | O3 | 99.025 | -2.133 | 2.03 |  |  |  |  |
|  |  | O4 | 97.311 | -2.209 | 1.923 |  |  |  |  |


| $\begin{aligned} & \text { CROSS } \\ & \text { SECTION } \end{aligned}$ | Distance from previous C.S. | POINT | N | E | Z | $\begin{aligned} & \text { D12 } \\ & \text { (cm) } \end{aligned}$ | $\begin{gathered} \text { D23 } \\ \text { (m) } \end{gathered}$ | $\begin{aligned} & \text { D34 } \\ & \text { (cm) } \end{aligned}$ | REMARKS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C.S. 16 | 150 | P1 | 102.731 | 3.156 | 2.754 | 140.4 | 9.305 | 66.3 |  |
|  |  | P2 | 101.751 | 2.15 | 2.692 |  |  |  |  |
|  |  | P3 | 92.561 | 0.693 | 2.147 |  |  |  |  |
|  |  | P4 | 92.024 | 0.304 | 2.251 |  |  |  |  |
| C.S. 17 | 160 | Q1 | 95.223 | 9.924 | 2.696 | 117.4 | 9.208 | 53.5 |  |
|  |  | Q2 | 94.445 | 9.045 | 2.564 |  |  |  |  |
|  |  | Q3 | 85.353 | 7.588 | 2.296 |  |  |  |  |
|  |  | Q4 | 85.121 | 7.106 | 2.404 |  |  |  |  |
| C.S. 18 | 170 | R1 | 87.56 | 16.334 | 2.476 | 119.1 | 9.627 | 97.3 |  |
|  |  | R2 | 86.8 | 15.417 | 2.472 |  |  |  |  |
|  |  | R3 | 77.363 | 13.512 | 2.385 |  |  |  |  |
|  |  | R4 | 77.006 | 12.607 | 2.408 |  |  |  |  |
| C.S. 19 | 180 | S1 | 79.534 | 22.438 | 2.376 | 109.7 | 9.599 | 1640 |  |
|  |  | S2 | 78.941 | 21.515 | 2.404 |  |  |  |  |
|  |  | S3 | 69.553 | 19.514 | 2.484 |  |  |  |  |
|  |  | S4 | 68.56 | 3.143 | 2.194 |  |  |  |  |
| C.S. 20 | 190 | T1 | 71.514 | 28.232 | 2.414 | 76.1 | 9.390 | 525.5 |  |
|  |  | T2 | 71.088 | 27.601 | 2.331 |  |  |  |  |
|  |  | T3 | 61.852 | 25.905 | 2.623 |  |  |  |  |
|  |  | T4 | 56.948 | 27.792 | 2.684 |  |  |  |  |
| C.S. 21 | 200 | U1 | 63.974 | 34.764 | 2.396 | 70.6 | 9.064 | 134.6 |  |
|  |  | U2 | 63.565 | 34.189 | 2.259 |  |  |  |  |
|  |  | U3 | 54.606 | 32.813 | 2.57 |  |  |  |  |
|  |  | U4 | 53.583 | 31.938 | 2.43 |  |  |  |  |
| C.S. 22 | 210 | V1 | 57.424 | 42.193 | 2.425 | 137.8 | 8.726 | 215.3 |  |
|  |  | V2 | 56.419 | 41.25 | 2.253 |  |  |  |  |
|  |  | V3 | 47.774 | 40.061 | 2.417 |  |  |  |  |
|  |  | V4 | 46.151 | 38.646 | 2.168 |  |  |  |  |
| C.S. 23 | 220 | W1 | 50.309 | 49.04 | 2.335 | 73.2 | 8.555 | 220.5 |  |
|  |  | W2 | 49.726 | 48.598 | 2.349 |  |  |  |  |
|  |  | W3 | 41.229 | 47.605 | 2.272 |  |  |  |  |
|  |  | W4 | 39.661 | 49.155 | 2.304 |  |  |  |  |




| $\begin{aligned} & \text { CROSS } \\ & \text { SECTION } \end{aligned}$ | Distance from previous C.S. | POINT | N | E | Z | $\begin{aligned} & \text { D12 } \\ & (\mathrm{cm}) \end{aligned}$ | $\begin{gathered} \text { D23 } \\ \text { (m) } \end{gathered}$ | $\begin{aligned} & \text { D34 } \\ & (\mathrm{cm}) \end{aligned}$ | REMARKS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C.S. 40 | 390 | OO1 | 3.313 | 59.409 | 3.738 | 137.0 | 26.000 | 177.7 | $\begin{gathered} \mathrm{D} 23 \text { is } \\ \text { increased } \\ \text { because of the } \\ \text { sharp curvature } \\ \text { at the police } \\ \text { barrier } \end{gathered}$ |
|  |  | OO2 | 2.325 | 60.358 | 3.741 |  |  |  |  |
|  |  | OO3 | 12.593 | 84.245 | 3.956 |  |  |  |  |
|  |  | OO4 | 10.985 | 85.002 | 4.007 |  |  |  |  |
| C.S. 41 | 400 | PP1 | 9.863 | 67.061 | 3.958 | 107.2 | 26.340 | 136.4 | $\begin{gathered} \text { D23 is } \\ \text { increased } \\ \text { because of the } \\ \text { sharp curvature } \\ \text { at the police } \\ \text { barrier } \end{gathered}$ |
|  |  | PP2 | 9.031 | 67.737 | 3.894 |  |  |  |  |
|  |  | PP3 | 17.934 | 92.527 | 4.077 |  |  |  |  |
|  |  | PP4 | 16.831 | 93.329 | 4.179 |  |  |  |  |
| C.S. 42 | 410 | QQ1 | 17.069 | 74.394 | 4.295 | 209.7 | 17.246 | 116.3 | $\begin{gathered} \text { D23 is } \\ \text { incrased } \\ \text { because of the } \\ \text { sharp curvature } \\ \text { at the police } \\ \text { barrier } \end{gathered}$ |
|  |  | QQ2 | 15.263 | 75.459 | 4.165 |  |  |  |  |
|  |  | QQ3 | 17.887 | 92.504 | 4.099 |  |  |  |  |
|  |  | QQ4 | 16.915 | 93.142 | 4.18 |  |  |  |  |
| C.S. 43 | 420 | RR1 | 23.182 | 82.585 | 4.428 | 241.3 | 17.837 | 79.0 | D23 isincreasedbecause of thesharp curvatureat the policebarrier |
|  |  | RR2 | 21.027 | 83.671 | 4.36 |  |  |  |  |
|  |  | RR3 | 22.597 | 101.439 | 4.223 |  |  |  |  |
|  |  | RR4 | 21.864 | 101.734 | 4.065 |  |  |  |  |
| C.S. 44 | 430 | SS1 | 30.56 | 85.626 | 4.59 | 144.3 | 18.184 | 137.4 | D23 isincreasedbecause of thesharp curvatureat the policebarrier |
|  |  | SS2 | 30.838 | 87.042 | 4.509 |  |  |  |  |
|  |  | SS3 | 46.042 | 97.017 | 4.549 |  |  |  |  |
|  |  | SS4 | 45.732 | 98.356 | 4.663 |  |  |  |  |
| C.S. 45 | 440 | TT1 | 40.481 | 87.686 | 4.608 | 98.9 | 18.562 | 166.5 | $\begin{gathered} \text { D23 is } \\ \text { increased } \\ \text { because of the } \\ \text { sharp curvature } \\ \text { at the police } \\ \text { barrier } \end{gathered}$ |
|  |  | TT2 | 40.323 | 88.662 | 4.574 |  |  |  |  |
|  |  | TT3 | 55.728 | 99.017 | 4.852 |  |  |  |  |
|  |  | TT4 | 55.558 | 100.673 | 4.935 |  |  |  |  |
| C.S. 46 | 450 | UU1 | 50.158 | 90.129 | 4.679 | 83.5 | 18.132 | 181.3 | D23 isincreasedbecause of thesharp curvatureat the policebarrier |
|  |  | UU2 | 49.985 | 90.946 | 4.623 |  |  |  |  |
|  |  | UU3 | 65.59 | 100.18 | 5.014 |  |  |  |  |
|  |  | UU4 | 65.6 | 101.993 | 5.137 |  |  |  |  |
| C.S. 47 | 460 | VV1 | 60.074 | 91.55 | 4.756 | 101.5 | 17.777 | 98.2 | $\begin{gathered} \text { D23 is } \\ \text { increased } \\ \text { because of the } \\ \text { sharp curvature } \\ \text { at the police } \\ \text { barrier } \end{gathered}$ |
|  |  | VV2 | 59.844 | 92.539 | 4.726 |  |  |  |  |
|  |  | VV3 | 75.618 | 100.737 | 5.159 |  |  |  |  |
|  |  | VV4 | 75.789 | 101.704 | 5.291 |  |  |  |  |


| $\begin{aligned} & \text { CROSS } \\ & \text { SECTION } \end{aligned}$ | Distance from previous C.S. | POINT | N | E | Z | $\begin{aligned} & \mathrm{D} 12 \\ & (\mathrm{~cm}) \end{aligned}$ | $\begin{gathered} \text { D23 } \\ \text { (m) } \end{gathered}$ | $\begin{aligned} & \text { D34 } \\ & (\mathrm{cm}) \end{aligned}$ | REMARK S |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C.S. 48 | 470 | WW1 | 23.964 | 88.603 | 4.434 | 77.9 | 17.301 | 79.5 | D23 inincreasedbecause of thesharpcurvature atte policebarrier |
|  |  | WW2 | 23.188 | 88.673 | 4.43 |  |  |  |  |
|  |  | WW3 | 18.659 | 105.371 | 4.792 |  |  |  |  |
|  |  | WW4 | 17.887 | 105.559 | 4.95 |  |  |  |  |
| C.S. 49 | 480 | XX1 | 25.458 | 98.363 | 4.626 | 53.2 | 17.248 | 72.4 | D23 isincreasedbecause of thesharpcurvature atthe policebarrier |
|  |  | XX2 | 24.937 | 98.469 | 4.628 |  |  |  |  |
|  |  | XX3 | 20.555 | 115.151 | 4.93 |  |  |  |  |
|  |  | XX4 | 19.837 | 115.245 | 4.895 |  |  |  |  |
| C.S. 50 | 490 | YY1 | 27.239 | 108.085 | 4.826 | 66.2 | 16.989 | 257.8 | D23 isincreasedbecause of thesharpcurvature atte policebarrier |
|  |  | YY2 | 26.644 | 108.376 | 4.838 |  |  |  |  |
|  |  | YY3 | 22.878 | 124.942 | 5.05 |  |  |  |  |
|  |  | YY4 | 20.302 | 125.041 | 5.143 |  |  |  |  |
| C.S. 51 | 500 | ZZ1 | 29.081 | 118.069 | 5.094 | 53.0 | 16.640 | 288.5 | D23 isincreasedbecause of thesharpcurvature atthe policebarrier |
|  |  | ZZ2 | 28.568 | 118.202 | 5.086 |  |  |  |  |
|  |  | ZZ3 | 25.355 | 134.529 | 5.413 |  |  |  |  |
|  |  | ZZ4 | 22.644 | 135.516 | 5.533 |  |  |  |  |
| C.S. 52 | 510 | AAA1 | 14.594 | 135.708 | 5.312 | 424.2 | 16.676 | 305.4 | D23 isincreasedbecause of thesharpcurvature atthe policebarrier |
|  |  | AAA2 | 14.963 | 131.482 | 5.411 |  |  |  |  |
|  |  | AAA3 | -0.061 | 124.246 | 5.804 |  |  |  |  |
|  |  | AAA4 | -0.082 | 121.192 | 5.976 |  |  |  |  |
| C.S. 53 | 520 | BBB1 | 4.801 | 134.36 | 5.658 | 273.5 | 16.385 | 50.2 | $\|$At point <br> BBB4, width <br> of truck is to <br> 193 <br> 17RUCK |
|  |  | BBB2 | 4.966 | 131.63 | 5.548 |  |  |  |  |
|  |  | BBB3 | -10.044 | 125.06 | 6.101 |  |  |  |  |
|  |  | BBB4 | -10.054 | 124.558 | 6.127 |  |  |  |  |
| C.S. 54 | 530 | CCC1 | -4.779 | 133.615 | 5.739 | 139.3 | 15.806 | 210.2 |  |
|  |  | CCC2 | -5.057 | 132.25 | 5.735 |  |  |  |  |
|  |  | CCC3 | -19.906 | 126.833 | 6.365 |  |  |  |  |
|  |  | CCC4 | -20.673 | 124.876 | 6.458 |  |  |  |  |
| C.S. 55 | 540 | DDD1 | -14.343 | 135.71 | 5.977 | 95.8 | 14.199 | 677.3 | $\begin{array}{\|c} \text { At point } \\ \text { DDDI width } \\ \text { truck is to be } \\ \text { ander to Do } \end{array}$ |
|  |  | DDD2 | -14.667 | 134.808 | 5.941 |  |  |  |  |
|  |  | DDD3 | -28.543 | 131.796 | 6.507 |  |  |  |  |
|  |  | DDD4 | -31.208 | 125.569 | 6.844 |  |  |  |  |


| $\begin{aligned} & \text { CROSS } \\ & \text { SECTION } \end{aligned}$ | Distance from previous C.S. | POINT | N | E | Z | $\begin{aligned} & \text { D12 } \\ & \text { (cm) } \end{aligned}$ | $\begin{gathered} \text { D23 } \\ \text { (m) } \end{gathered}$ | $\begin{aligned} & \text { D34 } \\ & (\mathrm{cm}) \end{aligned}$ | REMARKS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C.S. 56 | 550 | EEE1 | -23.365 | 139.771 | 6.185 | 114.1 | 14.874 | 269.0 |  |
|  |  | EEE2 | -23.893 | 138.76 | 6.277 |  |  |  |  |
|  |  | EEE3 | -38.094 | 134.335 | 6.814 |  |  |  |  |
|  |  | EEE4 | -39.957 | 132.394 | 6.937 |  |  |  |  |
| C.S. 57 | 560 | FFF1 | -29.723 | 147.538 | 6.289 | 410.7 | 13.387 | 160.8 |  |
|  |  | FFF2 | -32.216 | 144.274 | 6.341 |  |  |  |  |
|  |  | FFF3 | -45.223 | 141.106 | 6.934 |  |  |  |  |
|  |  | FFF4 | -46.493 | 140.12 | 6.76 |  |  |  |  |
| C.S. 58 | 570 | GGG1 | -36.4 | 157.723 | 6.739 | 854.9 | 11.700 | 108.1 |  |
|  |  | GGG2 | -40.2 | 150.065 | 6.596 |  |  |  |  |
|  |  | GGG3 | -51.835 | 148.829 | 6.954 |  |  |  |  |
|  |  | GGG4 | -52.684 | 148.16 | 7.639 |  |  |  |  |
| C.S. 59 | 580 | HHH1 | -43.428 | 160.871 | 6.735 | 281.1 | 12.185 | 116.9 |  |
|  |  | HHH2 | -45.463 | 158.932 | 6.778 |  |  |  |  |
|  |  | HHH3 | -57.49 | 156.978 | 6.989 |  |  |  |  |
|  |  | HHH4 | -58.464 | 156.332 | 6.946 |  |  |  |  |
| C.S. 60 | 590 | IIII | -46.561 | 165.547 | 7.22 | 277.7 | 10.743 | 114.7 |  |
|  |  | III2 | -49.096 | 166.681 | 7.243 |  |  |  |  |
|  |  | III3 | -51.838 | 177.068 | 7.1 |  |  |  |  |
|  |  | III4 | -52.776 | 177.728 | 6.975 |  |  |  |  |
| C.S. 61 | 600 | JJJ1 | -56.465 | 175.737 | 7.263 | 309.7 | 9.905 | 101.4 |  |
|  |  | JJJ2 | -59.012 | 173.975 | 7.505 |  |  |  |  |
|  |  | JJJ3 | -68.882 | 174.802 | 7.182 |  |  |  |  |
|  |  | JJJ4 | -69.796 | 174.364 | 7.1 |  |  |  |  |
| C.S. 62 | 620 | KKK1 | -70.644 | 190.847 | 8.452 | 251.1 | 10.536 | 50.6 |  |
|  |  | KKK2 | -72.166 | 188.85 | 7.747 |  |  |  |  |
|  |  | KKK3 | -82.692 | 189.317 | 7.591 |  |  |  |  |
|  |  | KKK4 | -83.083 | 188.996 | 7.528 |  |  |  |  |
| C.S. 63 | 640 | LLL1 | -86.209 | 203.132 | 7.95 | 25.9 | 11.256 | 69.3 |  |
|  |  | LLL2 | -86.374 | 202.933 | 7.949 |  |  |  |  |
|  |  | LLL3 | -97.625 | 202.599 | 8.113 |  |  |  |  |
|  |  | LLL4 | -98.026 | 202.034 | 7.963 |  |  |  |  |


| CROSS <br> SECTION | Distance from previous C.S. | POINT | N | E | Z | $\begin{aligned} & \mathrm{D} 12 \\ & (\mathrm{~cm}) \end{aligned}$ | $\begin{gathered} \text { D23 } \\ (\mathrm{m}) \end{gathered}$ | $\begin{aligned} & \text { D34 } \\ & \text { (cm) } \end{aligned}$ | REMARKS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C.S. 64 | 660 | MMM1 | -100.38 | 216.997 | 8.305 | 96.9 | 10.337 | 170.8 |  |
|  |  | MMM2 | -101.13 | 216.389 | 8.415 |  |  |  |  |
|  |  | MMM3 | -111.44 | 217.182 | 8.537 |  |  |  |  |
|  |  | MMM4 | -112.71 | 216.042 | 9.23 |  |  |  |  |
| C.S. 65 | 680 | NNN1 | -111.87 | 232.813 | 8.607 | 220.3 | 10.173 | 71.0 |  |
|  |  | NNN2 | -113.76 | 231.672 | 8.66 |  |  |  |  |
|  |  | NNN3 | -123.87 | 232.735 | 8.775 |  |  |  |  |
|  |  | NNN4 | -124.49 | 232.382 | 8.813 |  |  |  |  |
| C.S. 66 | 700 | OOO1 | -125.09 | 245.341 | 9.111 | 314.5 | 10.010 | 78.9 |  |
|  |  | 0002 | -122.07 | 246.24 | 9.001 |  |  |  |  |
|  |  | 0003 | -113.89 | 240.475 | 9.238 |  |  |  |  |
|  |  | OOO4 | -113.13 | 240.692 | 9.319 |  |  |  |  |
| C.S. 67 | 720 | PPP1 | -120.58 | 226.071 | 9.557 | 212.7 | 9.959 | 89.1 |  |
|  |  | PPP2 | -118.46 | 226.265 | 9.474 |  |  |  |  |
|  |  | PPP3 | -110.17 | 220.75 | 9.602 |  |  |  |  |
|  |  | PPP4 | -109.29 | 220.922 | 9.627 |  |  |  |  |
| C.S. 68 | 740 | QQQ1 | -116.04 | 206.724 | 9.696 | 139.5 | 10.386 | 141.3 |  |
|  |  | QQQ2 | -114.67 | 206.944 | 9.67 |  |  |  |  |
|  |  | QQQ3 | -105.86 | 201.434 | 9.885 |  |  |  |  |
|  |  | QQQ4 | -104.52 | 200.991 | 9.895 |  |  |  |  |
| C.S. 69 | 760 | RRR1 | -125.45 | 190.571 | 9.854 | 87.8 | 8.113 | 303.0 |  |
|  |  | RRR2 | -124.86 | 189.916 | 9.861 |  |  |  |  |
|  |  | RRR3 | -124.5 | 181.811 | 10.268 |  |  |  |  |
|  |  | RRR4 | -122.13 | 179.927 | 10.326 |  |  |  |  |
| C.S. 70 | 780 | SSS1 | -140.01 | 176.89 | 10.079 | 101.4 | 8.266 | 113.8 |  |
|  |  | SSS2 | -139.3 | 176.162 | 10.12 |  |  |  |  |
|  |  | SSS3 | -138.94 | 167.904 | 10.58 |  |  |  |  |
|  |  | SSS4 | -138.98 | 166.767 | 10.641 |  |  |  |  |
| C.S. 71 | 800 | TTT1 | -155.46 | 164.057 | 10.324 | 96.5 | 10.029 | 86.8 |  |
|  |  | TTT2 | -154.68 | 163.478 | 10.317 |  |  |  |  |
|  |  | TTT3 | -152.49 | 153.691 | 11.078 |  |  |  |  |
|  |  | TTT4 | -151.86 | 153.097 | 11.149 |  |  |  |  |


| $\begin{aligned} & \text { CROSS } \\ & \text { SECTION } \end{aligned}$ | Distance from previous C.S. | POINT | N | E | Z | $\begin{aligned} & \mathrm{D} 12 \\ & (\mathrm{~cm}) \end{aligned}$ | $\begin{gathered} \text { D23 } \\ \text { (m) } \end{gathered}$ | $\begin{aligned} & \text { D34 } \\ & \text { (cm) } \end{aligned}$ | REMARKS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C.S. 72 | 820 | UUU1 | -173.69 | 157.608 | 10.586 | 192.8 | 9.740 | 146.2 |  |
|  |  | UUU2 | -172.85 | 155.875 | 10.621 |  |  |  |  |
|  |  | UUU3 | -172.52 | 146.141 | 11.205 |  |  |  |  |
|  |  | UUU4 | -172.36 | 144.687 | 11.362 |  |  |  |  |
| C.S. 73 | 840 | VVV1 | -192.41 | 152.983 | 10.738 | 94.9 | 8.328 | 170.0 | C.S. 73 is marked <br> at 1.5 m ahead of <br> the junction <br> where the road is <br> bifercated to Shoghi's industrial area(road in direction) |
|  |  | VVV2 | -192.22 | 152.052 | 11.041 |  |  |  |  |
|  |  | VVV3 | -192.33 | 143.725 | 11.248 |  |  |  |  |
|  |  | VVV4 | -191.91 | 142.08 | 10.979 |  |  |  |  |
| C.S. 74 | 890 | WWW2 | -147.24 | 186.131 | 11.711 |  | 15.210 |  |  |
|  |  | WWW3 | -157.41 | 197.446 | 12.121 |  |  |  |  |
| C.S. 75 | 940 | XXX2 | -118.72 | 214.317 | 12.719 |  | 18.373 |  | C.S. 75 <br> Start of <br> Taxi Stand |
|  |  | XXX3 | -127.21 | 230.612 | 12.301 |  |  |  |  |
| C.S. 76 | 990 | YYY2 | -95.231 | 261.493 | 12.783 |  | 14.279 |  |  |
|  |  | YYY3 | -108.43 | 266.936 | 12.425 |  |  |  |  |
| C.S. 77 | 1040 | ZZZ2 | -107.53 | 305.534 | 13.329 |  | 9.394 |  |  |
|  |  | ZZZ3 | -116.87 | 306.549 | 13.476 |  |  |  |  |
| C.S. 78 | 1090 | AAAA2 | -122.56 | 346.295 | 14.334 |  | 11.074 |  |  |
|  |  | AAAA3 | -133.63 | 346.279 | 14.124 |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |

DETAILED OBSERVATION TABLE FROM THE LAYOUT

| STARTING CROSS SECTION | ENDING CROSS SECTION | Type-1 <br> FIXED <br> FIXED | Type-2 <br> FIXED <br> P.C. 1 | Type-3 <br> FIXED <br> P.C. 2 | $\begin{gathered} \text { Type-4 } \\ \text { FIXED } \\ \text { CANTILEVER } \end{gathered}$ | $\begin{gathered} \text { Type-5 } \\ \text { P.C. } 1 \\ \text { FIXED } \end{gathered}$ | $\begin{gathered} \text { Type-6 } \\ \text { P.C. } 1 \\ \text { P.C. } 1 \end{gathered}$ | $\begin{gathered} \text { Type-7 } \\ \text { P.C. } 1 \\ \text { P.C. } 2 \end{gathered}$ | $\begin{gathered} \text { Type-8 } \\ \text { P.C. } 1 \\ \text { CANTILEVER } \end{gathered}$ | $\begin{gathered} \text { Type-9 } \\ \text { P.C. } 2 \\ \text { FIXED } \end{gathered}$ | $\begin{array}{\|c} \text { Type-10 } \\ \text { P.C. } 2 \\ \text { P.C. } 1 \end{array}$ | $\begin{array}{\|c} \hline \text { Type-11 } \\ \text { P.C. } 2 \\ \text { P.C. } 2 \end{array}$ | Type-12 P.C. 2 <br> CANTILEVER | Type-13 CANTILEVER FIXED | $\begin{gathered} \text { Type-14 } \\ \text { CANTILEVER } \\ \text { P.C. } 1 \end{gathered}$ | Type-15 CANTILEVER P.C. 2 | Type-16 CANTILEVER CANTILEVER | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C.S. 1 | C.S. 2 | 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 |
| C.S. 2 | C.S. 3 | 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 |
| C.S. 3 | C.S. 4 | 1 | 1 |  |  |  |  | 1 |  |  |  | 1 | 1 |  |  |  |  | 5 |
| C.S. 4 | C.S. 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 5 |
| C.S. 5 | C.S. 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 5 |
| C.S. 6 | C.S. 7 |  | 1 |  |  | 1 |  |  |  |  | 1 | 1 |  |  |  | 1 |  | 5 |
| C.S. 7 | C.S. 8 | 3 | 1 |  |  | 1 | 1 |  |  |  |  |  |  |  |  |  |  | 6 |
| C.S. 8 | C.S. 9 | 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 |
| C.S. 9 | C.S. 10 | 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 |
| C.S. 10 | C.S. 11 | 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 |
| C.S. 11 | C.S. 12 | 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6 |
| C.S. 12 | C.S. 13 | 1 |  | 1 |  |  | 1 |  |  |  | 1 | 3 |  |  |  |  |  | 7 |
| C.S. 13 | C.S. 14 |  |  |  |  |  | 5 |  |  |  |  |  |  |  |  |  |  | 5 |
| C.S. 14 | C.S. 15 | 5 |  |  |  | 1 |  |  |  |  |  |  |  |  |  |  |  | 6 |
| C.S. 15 | C.S. 16 |  | 1 |  |  |  | 2 | 1 |  |  |  | 2 |  |  |  |  |  | 6 |
| C.S. 16 | C.S. 17 |  |  |  |  |  |  |  |  |  |  | 3 | 1 |  |  |  | 1 | 5 |
| C.S. 17 | C.S. 18 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 5 |
| C.S. 18 | C.S. 19 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 5 |
| C.S. 19 | C.S. 20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 5 |
| C.S. 20 | C.S. 21 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 5 |
| C.S. 21 | C.S. 22 |  |  |  |  |  |  |  |  |  |  | 1 |  |  |  | 1 | 3 | 5 |
| C.S. 22 | C.S. 23 |  |  |  |  |  |  |  |  |  |  |  | 1 |  |  |  | 4 | 5 |
| C.S. 23 | C.S. 24 | 1 |  |  |  | 1 |  |  |  |  | 1 | 1 |  |  |  | 1 |  | 5 |
| C.S. 24 | C.S. 25 | 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 |
| C.S. 25 | C.S. 26 | 2 |  | 1 |  |  |  |  |  |  |  | 2 |  |  |  |  |  | 5 |
| C.S. 26 | C.S. 27 |  |  |  |  |  | 2 |  |  |  | 1 | 2 |  |  |  |  |  | 5 |
| C.S. 27 | C.S. 28 |  |  |  |  |  |  | 1 |  |  |  | 1 | 1 |  |  |  | 2 | 5 |
| C.S. 28 | C.S. 29 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 5 |
| C.S. 29 | C.S. 30 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 5 |
| C.S. 30 | C.S. 31 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 5 |
| C.S. 31 | C.S. 32 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 5 |
| C.S. 32 | C.S. 33 | 3 |  |  |  |  |  |  |  | 1 | 1 |  |  |  |  | 1 |  | 6 |
| C.S. 33 | C.S. 34 | 2 | 1 |  |  |  |  | 1 |  |  |  |  |  |  |  |  |  | 4 |
| C.S. 34 | C.S. 35 | 4 |  |  |  | 1 |  |  |  |  | 1 |  |  |  |  |  |  | 6 |
| C.S. 35 | C.S. 36 | 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 |
| C.S. 36 | C.S. 37 | 3 | 1 |  |  |  | 2 | 1 |  |  |  | 1 |  |  |  |  |  | 8 |
| C.S. 37 | C.S. 38 |  |  |  |  |  |  |  |  |  |  | 4 |  |  |  |  |  | 4 |
| C.S. 38 | C.S. 39 |  |  |  |  |  |  |  |  |  |  | 6 |  |  |  |  |  | 6 |
| C.S. 39 | C.S. 40 |  |  |  |  |  |  |  |  |  |  | 5 |  |  |  |  |  | 5 |
| C.S. 40 | C.S. 41 |  |  |  |  |  |  |  |  |  |  | 1 | 1 |  |  |  | 3 | 5 |
| C.S. 41 | C.S. 42 |  |  |  |  | 1 | 1 |  |  |  | 1 | 1 |  |  |  | 1 |  | 5 |
| C.S. 42 | C.S. 43 | 4 | 1 |  |  |  |  | 1 |  |  |  |  |  |  |  |  |  | 6 |
| C.S. 43 | C.S. 44 |  |  |  |  |  |  |  |  |  |  | 4 |  |  |  |  |  | 4 |


| STARTING CROSS SECTION | ENDING CROSS SECTION | Type-1 FIXED FIXED | Type-2 <br> FIXED <br> P.C. 1 | Type-3 FIXED P.C. 2 | $\begin{gathered} \text { Type-4 } \\ \text { FIXED } \\ \text { CANTILEVER } \end{gathered}$ | Type-5 P.C. 1 <br> FIXED | $\begin{aligned} & \text { Type-6 } \\ & \text { P.C. } 1 \\ & \text { P.C. } 1 \end{aligned}$ | $\begin{aligned} & \text { Type-7 } \\ & \text { P.C. } 1 \\ & \text { P.C. } 2 \end{aligned}$ | $\begin{gathered} \text { Type-8 } \\ \text { P.C. } 1 \\ \text { CANTILEVER } \end{gathered}$ | $\begin{gathered} \text { Type-9 } \\ \text { P.C. } 2 \\ \text { FIXED } \end{gathered}$ | $\begin{array}{\|c\|} \hline \text { Type-10 } \\ \text { P.C. } 2 \\ \text { P.C. } 1 \end{array}$ | $\begin{array}{\|c\|} \hline \text { Type-11 } \\ \text { P.C. } 2 \\ \text { P.C. } 2 \end{array}$ | Type-12 P.C. 2 <br> CANTILEVER | Type-13 <br> CANTILEVER FIXED | $\begin{gathered} \text { Type-14 } \\ \text { CANTILEVER } \\ \text { P.C. } 1 \end{gathered}$ | Type-15 CANTILEVER P.C. 2 | Type-16 CANTILEVER CANTILEVER | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C.S. 44 | C.S. 45 |  |  |  |  |  |  |  |  |  |  | 1 | 1 |  |  |  | 3 | 5 |
| C.S. 45 | C.S. 46 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 5 |
| C.S. 46 | C.S. 47 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 5 |
| C.S. 47 | C.S. 48 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 5 |
| C.S. 48 | C.S. 49 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 9 | 9 |
| C.S. 49 | C.S. 50 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 5 | 5 |
| C.S. 50 | C.S. 51 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 9 | 9 |
| C.S. 51 | C.S. 52 | 4 |  |  |  | 1 | 1 |  |  |  | 1 | 1 |  |  |  | 1 | 4 | 13 |
| C.S. 52 | C.S. 53 | 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4 |
| C.S. 53 | C.S. 54 | 1 | 1 |  |  |  |  | 1 |  |  |  | 1 |  |  |  |  |  | 4 |
| C.S. 54 | C.S. 55 |  |  |  |  |  |  |  |  |  |  | 1 | 1 |  |  |  | 3 | 5 |
| C.S. 55 | C.S. 56 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1 | 4 | 5 |
| C.S. 56 | C.S. 57 | 4 |  |  |  | 1 |  |  |  |  | 1 |  |  |  |  |  |  | 6 |
| C.S. 57 | C.S. 58 | 6 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 6 |
| C.S. 58 | C.S. 59 | 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4 |
| C.S. 59 | C.S. 60 | 1 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2 |
| C.S. 60 | C.S. 61 | 3 |  |  |  | 1 |  |  | 1 |  | 1 |  |  |  |  | 1 | 1 | 8 |
| C.S. 61 | C.S. 62 | 10 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 10 |
| C.S. 62 | C.S. 63 | 1 | 1 |  |  |  | 1 | 1 |  |  |  | 1 | 1 |  |  |  | 4 | 10 |
| C.S. 63 | C.S. 64 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 10 | 10 |
| C.S. 64 | C.S. 65 |  |  |  |  | 1 | 2 |  |  |  | 1 | 1 |  |  |  | 1 | 1 | 7 |
| C.S. 65 | C.S. 66 | 8 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 8 |
| C.S. 66 | C.S. 67 | 7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 7 |
| C.S. 67 | C.S. 68 | 1 | 1 |  |  |  | 4 | 1 |  |  |  | 3 | 1 |  |  |  |  | 11 |
| C.S. 68 | C.S. 69 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 10 | 10 |
| C.S. 69 | C.S. 70 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 10 | 10 |
| C.S. 70 | C.S. 71 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 10 | 10 |
| C.S. 71 | C.S. 72 |  |  |  |  |  | 3 |  |  |  | 1 | 2 |  |  |  | 1 | 3 | 10 |
| C.S. 72 | C.S. 73 |  |  |  |  |  | 1 | 1 |  |  |  | 3 | 1 |  |  |  | 3 | 9 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | TOTAL | 124 | 11 | 2 | 0 | 10 | 26 | 10 | 1 | 1 | 12 | 53 | 10 | 0 | 0 | 10 | 167 | 437 |

## APPENDIX-D

## STAAD-EDITOR CODES

## 1. MODEL-1

## STAAD SPACE

START JOB INFORMATION
ENGINEER DATE 02-Apr-15
END JOB INFORMATION
INPUT WIDTH 79
UNIT METER KN
JOINT COORDINATES

$$
1000 ; 200 \text { 2; } 31.500 ; 41.50 \text { 2; } 50 \text {-0.3 0; } 60 \text {-0.3 2; } 71.5 \text {-0.3 0; }
$$

8 1.5-0.3 2; 90 -0.8 0; 100 -0.8 2; 11 1.5-0.8 0; 12 1.5-0.8 2;
13000.05 ; 141.500 .05 ; 15000.1 ; 16 1.500.1; 17000.15 ;
$181.500 .15 ; 19000.2 ; 201.500 .2 ; 21000.25 ; 221.500 .25$;
2300 0.3; 24 $1.500 .3 ; 25000.35 ; 261.500 .35 ; 27000.4 ; 281.500 .4$;
29000.45 ; 301.500 .45 ; 31000.5 ; 321.500 .5 ; 33000.55 ;
$341.500 .55 ; 35000.6 ; 361.500 .6 ; 37000.65 ; 381.500 .65$;
39000.7 ; 401.500 .7 ; 41000.75 ; 42 1.5 00.75 ; 43000.8 ; 44 1.5 00.8 ;
45000.85 ; 461.500 .85 ; 4700 0.9; 481.500 .9 ; 49000.95 ;
501.50 0.95; 51001 ; $521.501 ; 5300$ 1.05; 541.50 1.05; 5500 1.1;
561.50 1.1; 5700 1.15; 581.50 1.15; 5900 1.2; 601.50 1.2;

6100 1.25; 621.50 1.25; 6300 1.3; 641.50 1.3; 6500 1.35;
661.50 1.35; 6700 1.4; 681.50 1.4; 6900 1.45; 701.501 .45 ;

7100 1.5; 721.50 1.5; 7300 1.55; 741.50 1.55; 7500 1.6; 761.50 1.6;
7700 1.65; 781.50 1.65; 7900 1.7; 801.50 1.7; 8100 1.75;
821.50 1.75; 8300 1.8; 841.50 1.8; 8500 1.85; 861.501 .85 ;

8700 1.9; 881.50 1.9; 8900 1.95; 901.50 1.95;
MEMBER INCIDENCES
$515 ; 626 ; 737$; 84 8; 95 9; 106 10; 117 11; 128 12; 1313 ; 1524 ;

161 13; 173 14; 1813 15; 1914 16; 2013 14; 2115 17; 2216 18; 2315 16; 2417 19; 2518 20; 2617 18; 2719 21; 2820 22; $291920 ; 3021$ 23; 3122 24; 3221 22; 3323 25; 3424 26; 3523 24; 3625 27; 3726 28; 3825 26; 3927 29; 4028 30; 4127 28; 4229 31; 4330 32; 4429 30; 4531 33; 4632 34; 4731 32; 4833 35; 4934 36; 5033 34; 5135 37; 5236 38; 5335 36; 5437 39; 5538 40; 5637 38; 5739 41; 5840 42; 5939 40; 6041 43; 6142 44; 6241 42; 6343 45; 6444 46; 6543 44; 6645 47; 6746 48; 6845 46; 6947 49; 7048 50; 7147 48; 7249 51; 7350 52; 7449 50; 7551 53; 7652 54; 7751 52; 7853 55; 7954 56; 8053 54; 8155 57; 8256 58; 8355 56; 8457 59; 8558 60; 8657 58; 8759 61; 8860 62; 8959 60; 9061 63; 9162 64; 9261 62; 9363 65; 9464 66; 9563 64; 96 65 67; 9766 68; 9865 66; 9967 69; 10068 70; 10167 68; 10269 71; 1037072 ; $1046970 ; 1057173 ; 1067274$; 1077172 ; 1087375 ; 1097476 ; 11073 74; 1117577 ; $1127678 ; 1137576 ; 1147779 ; 11578$ 80; 1167778 ; 11779 81; 11880 82; 11979 80; 12081 83; 12182 84; $1228182 ; 1238385$; 12484 86; 12583 84; 12685 87; 12786 88; 12885 86; 12987 89; 13088 90; 13187 88; 13289 2; 13390 4; 13489 90;

DEFINE MATERIAL START
ISOTROPIC STEEL
E $2.05 \mathrm{e}+008$
POISSON 0.3
DENSITY 76.8195
ALPHA 1.2e-005
DAMP 0.03
ISOTROPIC CONCRETE
E $2.17185 \mathrm{e}+007$
POISSON 0.17
DENSITY 23.5616
ALPHA 1e-005
DAMP 0.05
END DEFINE MATERIAL
MEMBER PROPERTY INDIAN

9 TO 12 PRIS YD 0.3 ZD 0.3
MEMBER PROPERTY INDIAN
20232629323538414447505356596265687174778083868992 9598101104107110113116119122125128131134 PRIS YD 0.03 ZD 0.03 5 TO 8 TABLE ST ISJC150

1315 TO 19212224252728303133343637394042434546484951 52545557586061636466676970727375767879818284858788 90919394969799100102103105106108109111112114115117118 120121123124126127129130132133 TABLE ST ISA90X90X8 CONSTANTS

BETA 315 MEMB 1317192022232526282931323435373840414344

46474950525355565859616264656768707173747677798082 -
8385868889919294959798100101103104106107109110112113 -
115116118119121122124125127128130131133134
BETA 90 MEMB 78
BETA 270 MEMB 56
MATERIAL STEEL ALL
MATERIAL CONCRETE MEMB 9 TO 12

## SUPPORTS

9 TO 12 FIXED
LOAD 1 LOADTYPE None TITLE LOAD CASE 1
SELFWEIGHT Y-1 LIST 5 TO 1316 TO 134

## FLOOR LOAD

YRANGE 0 0.3 FLOAD -6 XRANGE 0 1.5 ZRANGE 02 GY
PERFORM ANALYSIS
PARAMETER 1
CODE IS800 LSD
CHECK CODE MEMB 5 TO 81315 TO 134
PARAMETER 2
CODE IS800 LSD

STEEL TAKE OFF LIST 5 TO 81315 TO 134
PERFORM ANALYSIS
FINISH

## 2. MODEL-2

STAAD SPACE
START JOB INFORMATION
ENGINEER DATE 02-Apr-15
END JOB INFORMATION
INPUT WIDTH 79
UNIT METER KN
JOINT COORDINATES
$1000 ; 2002 ; 31.500 ; 41.502 ; 50-0.30 ; 60-0.32 ; 70.75-0.30$;
80.75 -0.3 2; 90 -0.8 0; 100 -0.8 2; 110.75 -0.8 0; 120.75 -0.8 2;
$1110.7500 ; 1120.7502$ 2; 11300 1.95; 1141.50 1.95; 11500 1.9;
1161.50 1.9; 117001.85 ; 1181.501 .85 ; 11900 1.8; 1201.50 1.8;
121001.75 ; 1221.501 .75 ; 123001.7 ; 1241.501 .7 ; 125001.65 ;
$1261.501 .65 ; 12700$ 1.6; 1281.50 1.6; 12900 1.55; 1301.50 1.55;
13100 1.5; 1321.50 1.5; 13300 1.45; 1341.50 1.45; 13500 1.4;
1361.50 1.4; 13700 1.35; 1381.50 1.35; 13900 1.3; 1401.50 1.3; 14100 1.25; 1421.50 1.25; 14300 1.2; 1441.50 1.2; 14500 1.15; 1461.501 .15 ; 14700 1.1; 1481.50 1.1; 14900 1.05; 1501.501 .05 ; 151001 ; 1521.501 ; 153000.95 ; 1541.500 .95 ; 155000.9 ; 1561.500 .9 ; 157000.85 ; 1581.500 .85 ; 159000.8 ; 1601.500 .8 ; 161000.75 ; 1621.500 .75 ; 163000.7 ; 164 1.5 00.7 ; 165000.65 ;
1661.500 .65 ; 167000.6 ; 1681.500 .6 ; 169000.55 ; 1701.500 .55 ; 171000.5 ; 1721.500 .5 ; 173000.45 ; 1741.500 .45 ; 175000.4 ; $1761.500 .4 ; 177000.350001 ; 1781.500 .350001$; 179000.300001 ; 1801.500 .300001 ; 181000.250001 ; 1821.500 .250001 ; 183000.200001 ; 1841.500 .200001 ; 185000.150001 ; 1861.500 .150001 ; 187000.100001 ; $1881.500 .100001 ; 189000.0500008 ; 1901.500 .0500008$;

## MEMBER INCIDENCES

51 5; 62 6; 7111 7; 8112 8; 95 9; 106 10; 117 11; 128 12; 164111 3; 1668 4; 1673 7; 1681 189; 1693 190; 171113 2; 172114 4; 173113114 ;
174115 113; 175116 114; 176115 116; 177117 115; 178118 116; 179117118 ; 180119 117; 181120 118; 182119 120; 183121 119; 184122 120; 185121 122; 186123 121; 187124 122; 188123 124; 189125 123; 190126 124; 191125 126; 192127 125; 193128 126; 194127 128; 195129 127; 196130 128; 197129 130; 198131 129; 199132 130; 200131 132; 201133 131; 202134 132; 203133 134; 204135 133; 205136 134; 206135 136; 207137 135; 208138 136; 209137 138; 210139 137; 211140 138; 212139 140; 213141 139; 214142 140; 215141 142; 216143 141; 217144 142; 218143 144; 219145 143; 220146 144; 221145 146; 222147 145; 223148 146; 224147 148; 225149 147; 226150 148; 227149 150; 228151 149; 229152 150; 230151 152; 231153 151; 232154 152; 233153 154; 234155 153; 235156 154; 236155 156; 237157 155; 238158 156; 239157 158; 240159 157; 241160 158; 242159 160; 243161 159; 244162 160; 245161 162; 246163 161; 247164 162; 248163 164; 249165 163; 250166 164; 251165 166; 252167 165; 253168 166; 254167 168; 255169 167; 256170 168; 257169 170; 258171 169; 259172 170; 260171 172; 261173 171; 262174 172; 263173 174; 264175 173; 265176 174; 266175 176; 267177 175; 268178 176; 269177 178; 270179 177; 271180 178; 272179 180; 273181 179; 274182 180; 275181 182; 276183 181; 277184 182; 278183 184; 279185 183; 280186 184; 281185 186; 282187 185; 283188 186; 284187 188; 285189 187; 286190 188; 287189 190; 2881 111; 2894 112; 290112 2;

## DEFINE MATERIAL START

ISOTROPIC STEEL
E $2.05 \mathrm{e}+008$
POISSON 0.3
DENSITY 76.8195
ALPHA 1.2e-005
DAMP 0.03
ISOTROPIC CONCRETE

E $2.17185 \mathrm{e}+007$
POISSON 0.17
DENSITY 23.5616
ALPHA 1e-005
DAMP 0.05
END DEFINE MATERIAL
MEMBER PROPERTY INDIAN
9 TO 12 PRIS YD 0.3 ZD 0.3
MEMBER PROPERTY INDIAN
5 TO 8 TABLE ST ISJC150
MEMBER PROPERTY INDIAN
173176179182185188191194197200203206209212215218221224227

230233236239242245248251254257260263266269272275278281284

287 PRIS YD 0.03 ZD 0.03
164166 TO 169171172174175177178180181183184186187189190192

193195196198199201202204205207208210211213214216217219220

222223225226228229231232234235237238240241243244246247249

250252253255256258259261262264265267268270271273274276277

279280282283285286288 TO 290 TABLE ST ISA90X90X8 CONSTANTS

BETA 135 MEMB 166167
BETA 180 MEMB 8
BETA 0 MEMB 7
BETA 270 MEMB 56

BETA 315 MEMB 164169172175178181184187190193196199202205 208-

211214217220223226229232235238241244247250253256259262265

268271274277280283286288 TO 290
MATERIAL STEEL MEMB 5 TO 8164166 TO 169171 TO 290
MATERIAL CONCRETE MEMB 9 TO 12
SUPPORTS
9 TO 12 FIXED
LOAD 1 LOADTYPE None TITLE LOAD CASE 1
SELFWEIGHT Y-1 LIST 5 TO 12164166 TO 169171 TO 290
FLOOR LOAD
YRANGE 0 0.3 FLOAD -6 XRANGE 0 1.5 ZRANGE 02 GY
PERFORM ANALYSIS
PARAMETER 1
CODE IS800 LSD
CHECK CODE MEMB 5 TO 8164166 TO 169171 TO 290
PARAMETER 2
CODE IS800 LSD
GROUP MEMB 5 TO 8
PARAMETER 3
CODE IS800 LSD
GROUP MEMB 164
PARAMETER 4
CODE IS800 LSD
GROUP MEMB 166167
PARAMETER 7
CODE IS800 LSD
STEEL TAKE OFF LIST 5 TO 8164166 TO 169171 TO 290
PERFORM ANALYSIS
FINISH

## 3. MODEL-3

## STAAD SPACE

## START JOB INFORMATION

## ENGINEER DATE 02-Apr-15

## END JOB INFORMATION

## INPUT WIDTH 79

UNIT METER KN

## JOINT COORDINATES

$1000 ; 200$ 2; 31.500 ; 41.50 2; 50 -0.3 0; 60 -0.3 2; 90 - 0.80 ; 100 -0.8 2; 1130 -1.5 0; $1140-1.52 ; 115000.05 ; 1161.500 .05$;
117000.1 ; 1181.500 .1 ; 119000.15 ; 1201.500 .15 ; 121000.2 ;
1221.500 .2 ; 123000.25 ; 1241.500 .25 ; 125000.3 ; 1261.500 .3 ;
127000.35 ; 1281.500 .35 ; 129000.4 ; 1301.500 .4 ; 131000.45 ;
$1321.500 .45 ; 133000.5 ; 1341.500 .5 ; 135000.55$; 1361.500 .55 ;
137000.6 ; 1381.500 .6 ; 139000.65 ; 1401.500 .65 ; 141000.7 ;
1421.500 .7 ; 143000.75 ; 1441.500 .75 ; 145000.8 ; 1461.500 .8 ;
147000.85 ; 1481.500 .85 ; 149000.9 ; 1501.500 .9 ; 151000.95 ;
$1521.500 .95 ; 153001$; 1541.501 ; $155001.05 ; 1561.501 .05$;

15700 1.1; 1581.50 1.1; 15900 1.15; 1601.50 1.15; 16100 1.2;
1621.50 1.2; 163001.25 ; 1641.501 .25 ; 16500 1.3; 1661.50 1.3;
$167001.35 ; 1681.501 .35 ; 169001.4 ; 1701.501 .4$; 171001.45 ;
$1721.501 .45 ; 173001.5 ; 1741.501 .5 ; 175001.55$; 1761.501 .55 ;
$177001.6 ; 1781.501 .6 ; 17900$ 1.65; 1801.50 1.65; 18100 1.7;
1821.501 .7 ; 183001.75 ; 1841.501 .75 ; 185001.8 ; 1861.50 1.8;

18700 1.85; 1881.50 1.85; 18900 1.9; 1901.50 1.9; 191001.95 ;
1921.501 .95 ;

## MEMBER INCIDENCES

$515 ; 626 ; 959 ; 10610 ; 1681144 ; 170113$ 3; 17113 ; 17224 ;

1731 115; 1743 116; 175115 117; 176116 118; 177115 116; 178117119 ; 179118 120; 180117 118; 181119 121; 182120 122; 183119 120; 184121 123; 185122 124; 186121 122; 187123 125; 188124 126; 189123 124; 190125 127; 191126 128; 192125 126; 193127 129; 194128 130; 195127 128; 196129 131; 197130 132; 198129 130; 199131 133; 200132 134; 201131 132; 202133135 ; 203134 136; 204133 134; 205135 137; 206136 138; 207135 136; 208137 139; 209138 140; 210137 138; 211139 141; 212140 142; 213139 140; 214141 143; 215142 144; 216141 142; 217143 145; 218144 146; 219143 144; 220145 147; 221146 148; 222145 146; 223147 149; 224148 150; 225147 148; 226149 151; 227150 152; 228149 150; 229151 153; 230152 154; 231151 152; 232153155 ; 233154 156; $234153154 ; 235155$ 157; 236156 158; 237155 156; 238157 159; 239158 160; 240157 158; 241159 161; 242160 162; 243159 160; 244161 163; 245162 164; 246161 162; 247163 165; 248164 166; 249163 164; 250165 167; 251166 168; 252165 166; 253167 169; 254168 170; 255167 168; 256169 171;

257170 172; 258169 170; 259171 173; 260172 174; 261171 172; 262173 175; 263174 176; 264173 174; 265175 177; 266176 178; 267175 176; 268177 179; 269178 180; 270177 178; 271179 181; 272180 182; 273179 180; 274181 183; 275182 184; 276181 182; 277183 185; 278184 186; 279183 184; 280185 187; 281186 188; 282185 186; 283187 189; 284188 190; 285187 188; 286189 191; 287190 192; 288189 190; 289191 2; 290192 4; 291191 192;

DEFINE MATERIAL START
ISOTROPIC STEEL

E $2.05 \mathrm{e}+008$

POISSON 0.3

DENSITY 76.8195

ALPHA 1.2e-005

DAMP 0.03
ISOTROPIC CONCRETE

E $2.17185 \mathrm{e}+007$

POISSON 0.17

DENSITY 23.5616

ALPHA 1e-005

DAMP 0.05
END DEFINE MATERIAL

MEMBER PROPERTY INDIAN

910 PRIS YD 0.3 ZD 0.3
MEMBER PROPERTY INDIAN

177180183186189192195198201204207210213216219222225228231

234237240243246249252255258261264267270273276279282285288
-

291 PRIS YD 0.03 ZD 0.03

168170 TO 176178179181182184185187188190191193194196197199 -

200202203205206208209211212214215217218220221223224226227

229230232233235236238239241242244245247248250251253254256

257259260262263265266268269271272274275277278280281283284

286287289290 TABLE ST ISA90X90X8
56 TABLE ST ISJC150
CONSTANTS

BETA 225 MEMB 170

BETA 135 MEMB 168

BETA 270 MEMB 56

BETA 45 MEMB 172173175178181184187190193196199202205208 211214 -

217220223226229232235238241244247250253256259262265268271

274277280283286289

BETA 315 MEMB 171174176177179180182183185186188189191192 194 -

195197198200201203204206207209210212213215216218219221222
-

224225227228230231233234236237239240242243245246248249251

252254255257258260261263264266267269270272273275276278279

281282284285287288290291

MATERIAL STEEL MEMB 56168170 TO 291

MATERIAL CONCRETE MEMB 910

SUPPORTS

910113114 FIXED

LOAD 1 LOADTYPE None TITLE LOAD CASE 1

SELFWEIGHT Y -1 LIST 56910168170 TO 291

FLOOR LOAD

YRANGE 0 0.3 FLOAD -6 XRANGE 0 1.5 ZRANGE 02 GY

PERFORM ANALYSIS

PARAMETER 1

CODE IS800 LSD

CHECK CODE MEMB 56168170 TO 291

PARAMETER 2
CODE IS800 LSD
GROUP MEMB 56

PARAMETER 3
CODE IS800 LSD

GROUP MEMB 168170

STEEL TAKE OFF LIST 56168170 TO 291

PERFORM ANALYSIS

FINISH

## 4. GUARD RAIL

STAAD SPACE
START JOB INFORMATION
ENGINEER DATE 13-May-15
END JOB INFORMATION
INPUT WIDTH 79
UNIT METER KN
JOINT COORDINATES
$1000 ; 200.30 ; 301.30 ; 40.10 .30 ; 50.11 .30 ; 60.20 .30$;
$70.21 .30 ; 80.30 .30 ; 90.31 .30 ; 100.40 .30 ; 110.41 .30$;
$120.50 .30 ; 130.51 .30 ; 140.60 .30 ; 150.61 .30 ; 160.70 .30$;
$170.71 .30 ; 180.80 .30 ; 190.81 .30 ; 200.90 .30 ; 210.91 .30$;
$2210.30 ; 2311.30 ; 241.10 .30 ; 251.11 .30 ; 261.20 .30 ; 271.21 .30 ;$
281.30 .3 0; $291.31 .30 ; 301.40 .30 ; 311.41 .30 ; 321.50 .30$;
$331.51 .30 ; 341.60 .30 ; 351.61 .30 ; 361.70 .30 ; 371.71 .30$;
$381.80 .30 ; 391.81 .30 ; 401.90 .30 ; 411.91 .30 ; 42200 ; 4320.30$;
4421.30 ;

MEMBER INCIDENCES
$112 ; 223 ; 324 ; 435 ; 545 ; 646 ; 757 ; 867 ; 968 ; 1079 ; 1189$;
128 10; $13911 ; 141011 ; 151012 ; 161113 ; 171213 ; 181214 ; 191315$;
2014 15; 2114 16; 2215 17; 2316 17; 2416 18; 2517 19; 2618 19; 2718 20; 2819 21; 2920 21; 302022 ; 3121 23; 3222 23; 3322 24; 3423 25; 352425 ;
3624 26; 3725 27; 3826 27; 3926 28; 4027 29; 4128 29; 4228 30; 4329 31;
4430 31; 4530 32; 4631 33; 4732 33; 4832 34; 4933 35; 5034 35; 513436 ;
5235 37; 5336 37; 5436 38; 5537 39; 5638 39; 5738 40; 5839 41; 594041 ;
6042 43; 6140 43; 6241 44; 6343 44;
DEFINE MATERIAL START
ISOTROPIC STEEL
E $2.05 \mathrm{e}+008$
POISSON 0.3
DENSITY 76.8195
ALPHA 1.2e-005
DAMP 0.03
END DEFINE MATERIAL
MEMBER PROPERTY INDIAN
1 TO 4679101213151618192122242527283031333436373940 -
42434546484951525455575860 TO 63 TABLE ST ISA50X50X5
MEMBER PROPERTY INDIAN
581114172023262932353841444750535659 PRIS YD 0.025
CONSTANTS
BETA 45 MEMB 1247101316192225283134374043464952555862
BETA 135 MEMB 369121518212427303336394245485154576061 63

MATERIAL STEEL ALL
SUPPORTS
142 FIXED
LOAD 1 LOADTYPE None TITLE LOAD CASE 1

SELFWEIGHT Y-1 LIST 1 TO 63
PERFORM ANALYSIS
PARAMETER 1
CODE IS800 LSD
CHECK CODE ALL
PARAMETER 2
CODE IS800 LSD
STEEL TAKE OFF LIST 1 TO 63
PERFORM ANALYSIS
FINISH

