



# Ultra-Wideband Compact Circularly Polarized Antenna

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## Abstract

In this research work, a circularly polarized (CP) monopole antenna is designed for Ultra-Wideband (UWB) applications. The CP UWB antenna is made up of a reformed ring patch and ground plane. The slots and stubs are inserted in the ground to achieve CP in the UWB antenna. This antenna attained an Axial Ratio Bandwidth (ARBW) of 5 GHz (4.0–9.0 GHz) that lies in the UWB frequency range that is from 3.1 to 10.6 GHz. The designed antenna has a radiation efficiency of around 80% for the complete UWB frequency range. The CP UWB antenna is designed and fabricated using the FR4 with a compact size of  $32 \times 30 \times 1.6 \text{ mm}^3$  and with a peak gain of 6.8 dBi. Tested results are in good resemblance with simulated ones.

**Keywords** Ultra-wide band (UWB) · Circular polarization (CP) · Impedance bandwidth (IB) · Axial ratio bandwidth (ARBW) · Compact size

## 1 Introduction

Ultra-Wide Band (UWB) technology is used in most of the communication systems because of wide Impedance Bandwidth (IB), simple fabrication method, low power dissipation, higher transmission data rates, low cost, multipath cancellation. The UWB [1–5] ranges from 3.1 to 10.6 GHz is used for numerous wireless applications. The biggest challenge for wireless communication systems is the polarization mismatch loss between the transmitter and the receiver [6]. To overcome the polarization mismatch loss and multipath interference it is essential to propose a UWB antenna with circular polarization (CP) features. In general, compared to the linearly polarized antenna, the circularly polarized antenna has many advantages such as eliminating polarization mismatch and reducing multipath interference [7]. Normally, CP wave in the UWB antenna can be produced by two orthogonally placed electric fields or magnetic fields with identical amplitude and 90° phase difference. Different techniques are used to generate the CP wave in the UWB antenna such as by employing couplers, phase shifters, or modified antenna structures. With the growing demand for the CP UWB antenna, the ARBW of the CP antenna required to be improved. A CP antenna can be obtained by using two feeding techniques: single feed

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and multi-feed. For ease, we have chosen a single fed monopole antenna. With the growing demand CP UWB antenna for high data wireless communication systems, the ARBW needs to enhance. Although the impedance bandwidth of the single fed monopole antenna is small due to the high Q factor of the antenna [8]. Therefore, designing a compact single fed monopole antenna with a wide axial ratio is a great task. Further, to obtain wide ARBW different stub [8] and slots [9] is reported in the literature. Various CP Antenna with different patch shape, for example, S-model [10], arc-slot antenna [11] and X-shaped [12], meandered- [13], hook [14], modified circular ring [15] antenna has been also suggested with wide 3 dB ARBW. In this editorial, a ring-shaped planar antenna is suggested with wide ARBW. A slot is etched under the feed line and the strip is extended from the ground to obtain a wider axial ratio. The proposed antenna has impedance bandwidth of 3–11 GHz, whereas the ARBW is 4–9 GHz. Further, the entire ARBW is coincided by impedance bandwidth, thus CP characteristics are satisfactory for the suggested antenna. In the interim, the suggested antenna has a simpler compact size with wider ARBW than the above-mentioned antenna. The design process and measured outcomes are analyzed and discussed in detail in the succeeding divisions.

## 2 Circular Polarized UWB Antenna

### 2.1 Design and Analysis

Figure 1 depicts the layout of the CP UWB antenna. The suggested structure comprises of the ring-shaped patch with the outer and inner radius of  $R_1$  and  $R_2$ , respectively, Table 1 presents the dimension of the suggested CP UWB Antenna. A slot and stub are incorporated in the ground to enhance the ARBW. The proposed structure is simulated and fabricated using FR-4 substrate whose  $\epsilon_r$  is 4.4 and height (h) is 1.6 mm Ansoft HFSS v.13 software is used to simulate the suggested antenna. EP 2006 PCB Prototype machine is used to fabricated the suggested antenna. The antenna parameters like S parameters and radiation pattern are evaluated using the Agilent N5230C vector network analyzer and microwave shield anechoic chamber respectively. Figure 2 indicates the archetype of the circularly polarized UWB antenna. The measured and simulated VSWR is depicted in Fig. 3.

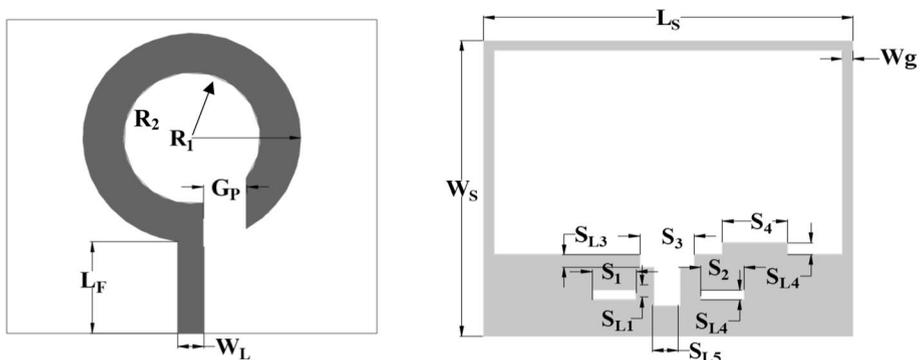
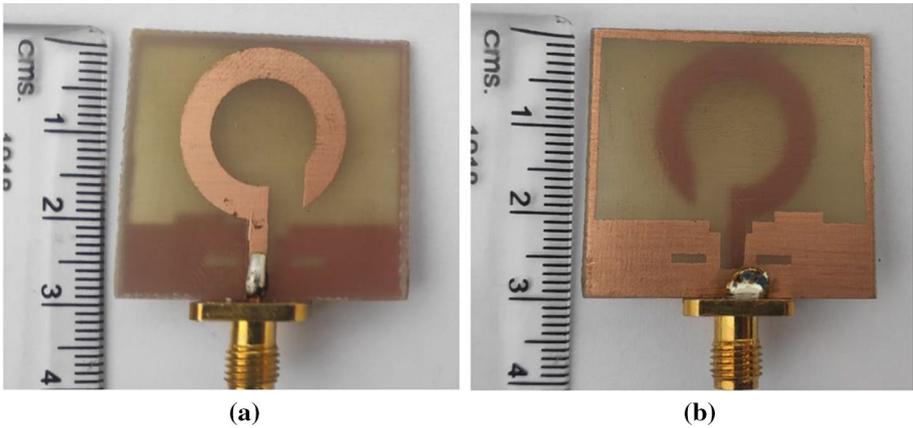


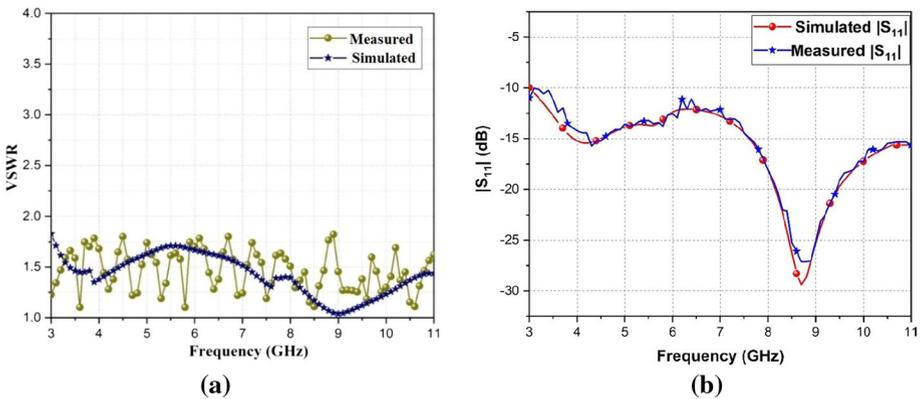
Fig. 1 Proposed Circular polarized ultra wide band antenna

**Table 1** Dimensions of suggested antenna

Parameter	$S_3$	$S_{L,3}$	$S_2$
Units (mm)	5	1.3	4
Parameter	$S_{L,2}$	$S_1$	$S_{L,1}$
Units (mm)	1	1	4
Parameter	$S_{L,4}$	$S_4$	$L_G$
Units (mm)	1.2	4	8.3
Parameter	$S_{L,5}$	$G_P$	$L_F$
Units (mm)	5	4	8.7
Parameter	$W_s$	$L_s$	$W_L$
Units (mm)	34	30	2.4
Parameter	$R_1$	$R_2$	$G_P$
Units (mm)	10	6.3	4

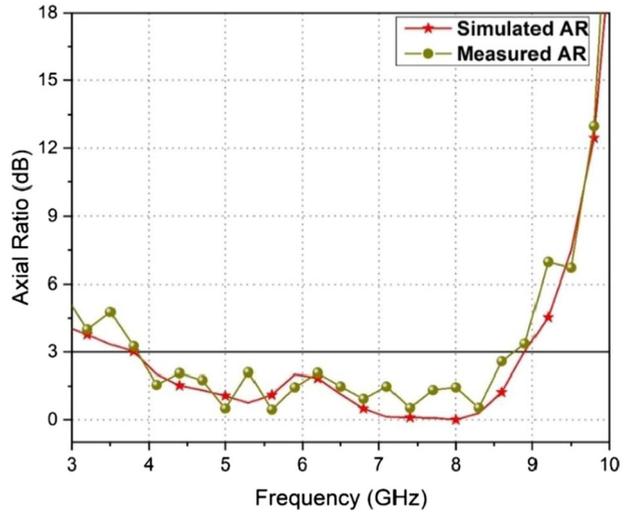


**Fig. 2** **a** Uppermost view, **b** Foot view



**Fig. 3** Tested and simulated VSWR and return loss

**Fig. 4** Tested and simulated Axial ratio



**Fig. 5** Variation of VSWR for different ring slot width ( $G_p$ )

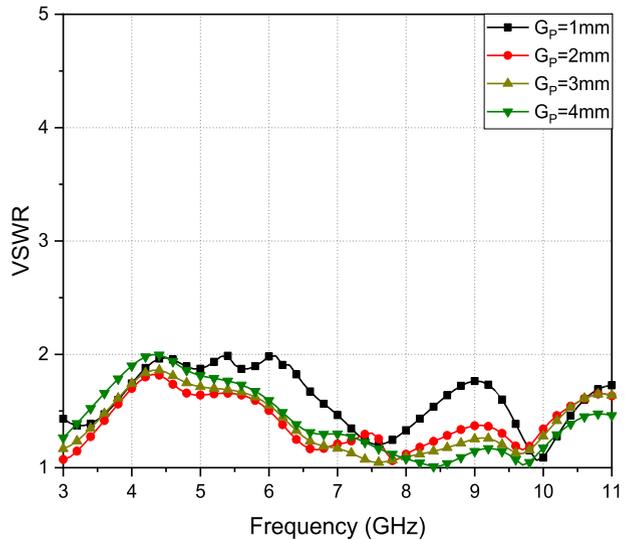
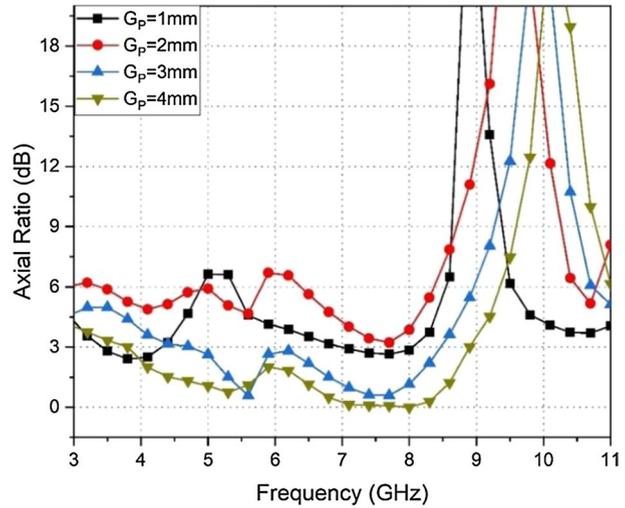


Figure 4 displays the deviation of the simulated and tested axial ratio with frequency. It can be seen that 3 dB ARBW of the suggested structure is 4–9 GHz coincided by 10 dB impedance bandwidth. Figures 5 and 6, shows that, it has marginal effect on impedance matching, although by increasing slot length from  $S_1 = 1\text{--}4$  mm, the upper band of the axial ratio moves from 7.6 to 9 GHz, which increases overall ARBW.

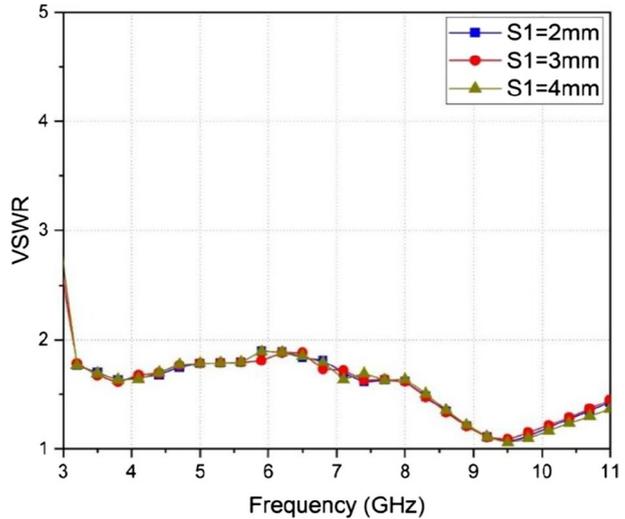
**2.2 Variations in the ground slot( $S_1$ )**

Figures 7 and 8 depict the simulated VSWR and axial ratio for different values of  $S_1 = 2, 3,$  and 4 mm respectively. It is observed that there is a negligible variation on

**Fig. 6** Axial ratio for different ring slot width( $G_p$ )

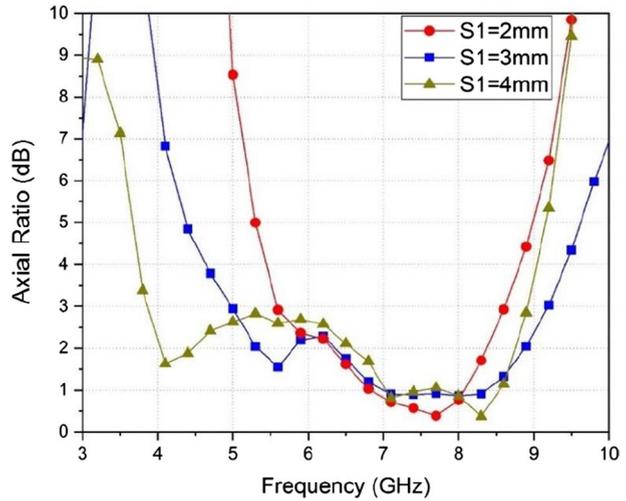


**Fig. 7** Deviation of VSWR for dissimilar ground slot length ( $S_1$ )

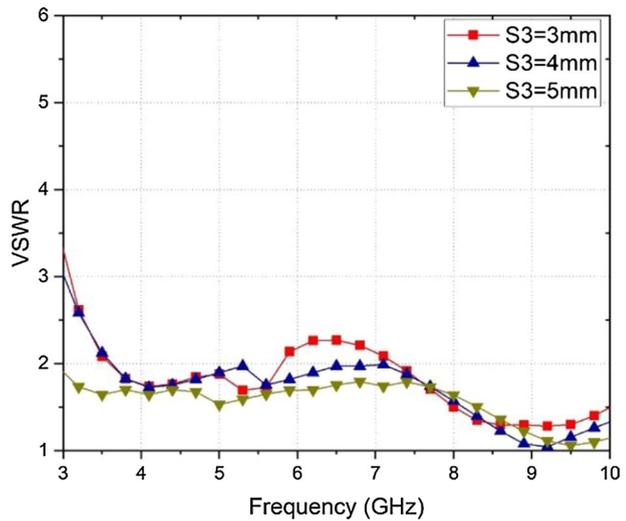


VSWR, whereas, in Fig. 8, significant variation is seen in the Axial ratio for different ground slot which improves overall ARBW length ( $S_1$ ). As the slot length increased from  $S_1 = 2\text{--}4$  mm, the lower band of the axial ratio moves from 5.5 to 4 GHz. By varying  $S_2$  the same variation is observed in VSWR and the axial ratio of the suggested CP UWB antenna.

**Fig. 8** Deviation of Axial ratio for dissimilar ground slot length ( $S_1$ )



**Fig. 9** Deviation of VSWR for dissimilar the slots length ( $S_3$ )

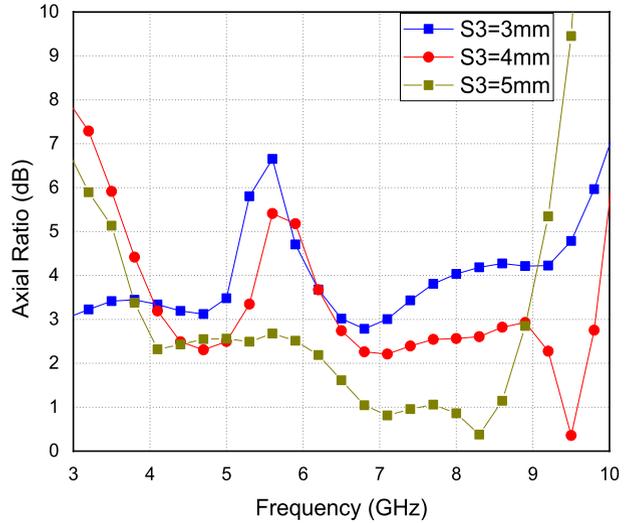


### 2.3 Variation of the slot length( $S_3$ )

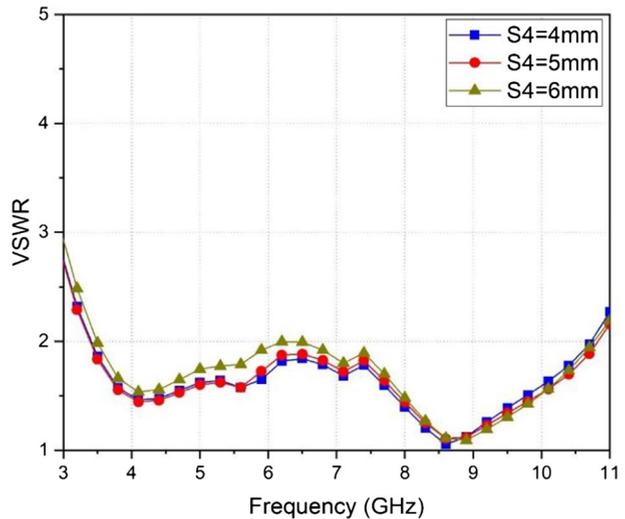
Figure 9 indicates the deviation of VSWR for different slot lengths ( $S_3$ ). It is seen that there is a little deviation on impedance matching, as slot length  $S_3$  increase from 3 to 5 mm.

Figure 10. presents the deviation of the axial ratio with frequency. Two CP mode approaches each other as  $S_3$  decrease to 5 mm and proposed structure shows the maximum bandwidth of AR. Thus, the two CP modes get unite by varying the length of the slot.

**Fig.10** Deviation of Axial Ratio for dissimilar the slots length ( $S_3$ )



**Fig.11** Deviation of VSWR for dissimilar ground slot length ( $S_4$ )

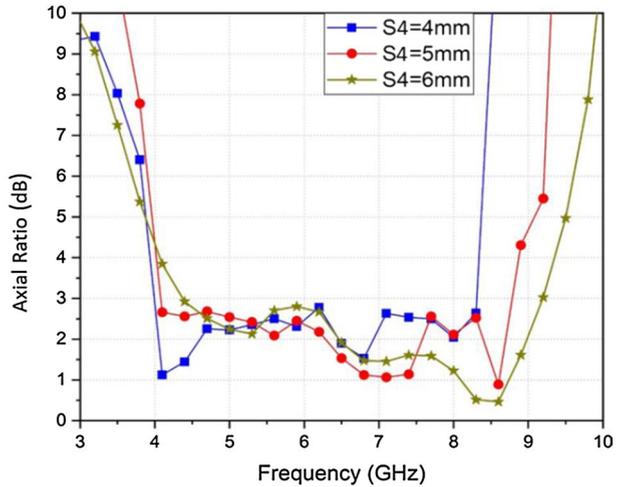


**2.4 Variations in the ground slot( $S_4$ )**

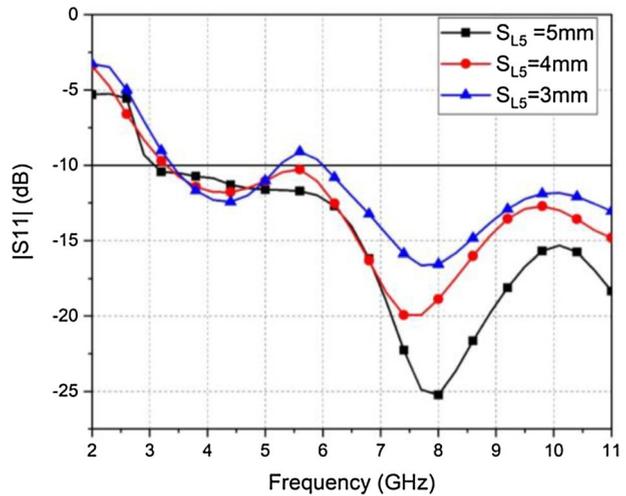
Figure 11 indicates the deviation of VSWR with frequency for different ground slot lengths ( $S_4$ ). It is perceived that there is a minimal variation on VSWR, whereas, in Fig. 12, significant variation is seen in the axial ratio for different ground slot length ( $S_4$ ). As the slot length increased from  $S_4=4-6$  mm, the upper band of the axial ratio moves from 8.3 to 9.1 GHz, which improves the overall ARBW.

Figures 13 and 14 indicates the deviation of return loss and axial ratio for different ground slot lengths ( $S_{L5}$ ). It is perceived that there is significant variation on both return loss and axial ratio. As the slot length increased from  $S_4=3-5$  mm, the return loss and axial ratio improves significantly. To understand the circular polarization mechanism the surface current distribution is analyzed with phase change from  $0^\circ$  to  $270^\circ$ . The current

**Fig. 12** Deviation of Axial ratio for dissimilar ground slot length ( $S_4$ )



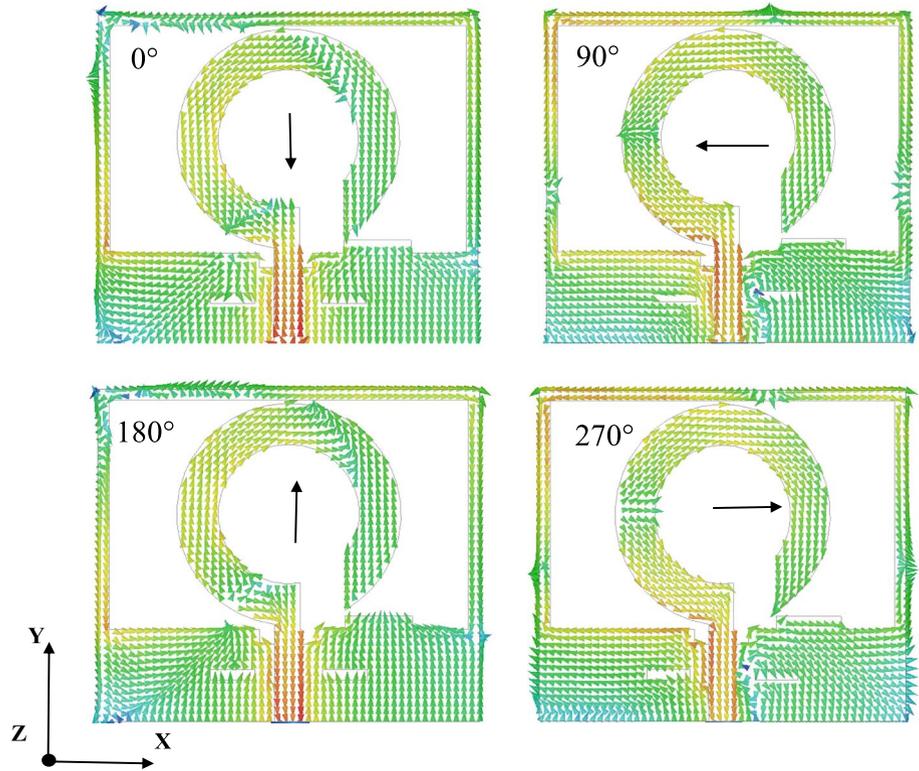
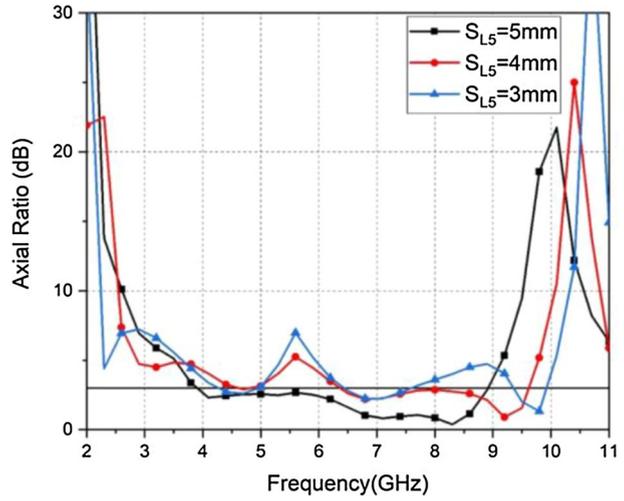
**Fig. 13** Deviation of return loss for dissimilar ground slot length ( $S_{L5}$ )



circulations of the proposed structure at 5.5 GHz at dissimilar time pause:  $w(t)=0^\circ, 90^\circ, 180^\circ,$  and  $270^\circ$  is demonstrated in Fig. 15. The predominant vector direction is in  $-Y$  direction for  $0^\circ$ , while for  $90^\circ$  the predominant vector direction is  $-X$  direction. For  $180^\circ$  and  $270^\circ$ , the predominant vector direction is reverse to  $0^\circ$  and  $90^\circ$ . It is observed from the figure that as the phase increase from  $0^\circ$  to  $270^\circ$ , with the identical amplitude and  $90^\circ$  phase difference the current moves in the left-handed or clockwise direction, as observed from the  $+Z$  direction. Thus, it is noticed that the suggested circularly polarized UWB antenna can radiate left-hand CP (LHCP) wave as observed from  $+Z$  direction and right-hand CP (RHCP) from the  $-Z$  direction. Figure 16 indicates the simulated and tested H plane and E plane at 5 GHz and 7 GHz. In  $+Z$  direction the radiated wave is LHCP and in the  $-Z$  direction the radiated wave is RHCP.

Figure 17 illustrates the radiation efficiency of the suggested CP UWB antenna. Fig. 18 indicates the gain variation with the frequency of the suggested antenna. Good constancy can

**Fig. 14** Deviation of Axial ratio for dissimilar ground slot length ( $S_{L5}$ )



**Fig. 15** Current density at 6 GHz with the dissimilar phase of  $0^\circ$ ,  $90^\circ$ ,  $180^\circ$ , and  $270^\circ$

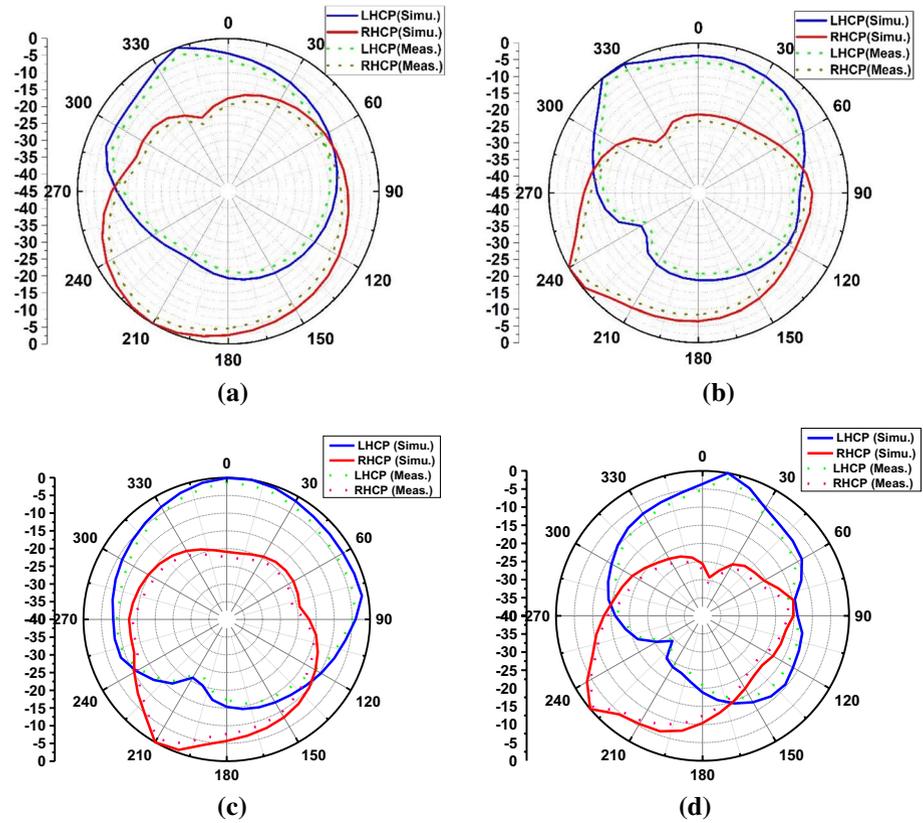
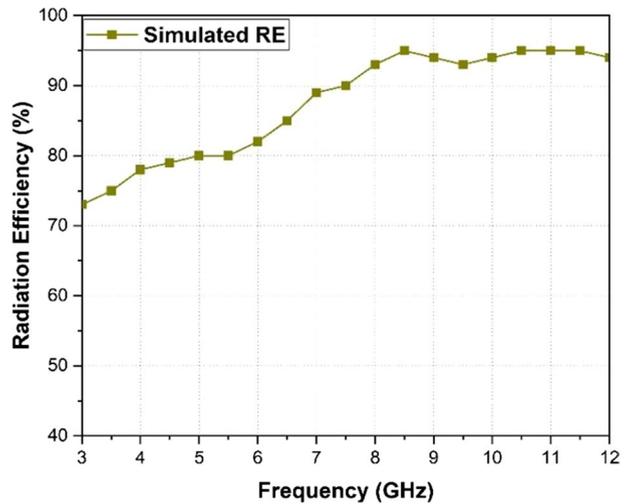
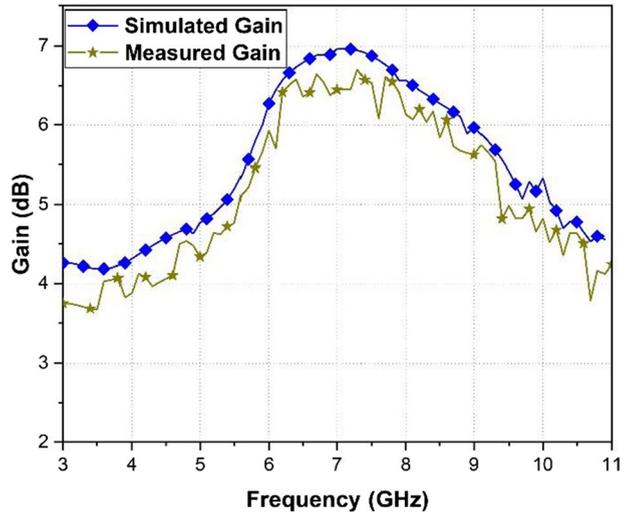


Fig. 16 Radiation plot a E-plane and b H-plane at 5 GHz c E-plane and d H-plane at 7 GHz

Fig. 17 The plot of radiation efficiency



**Fig. 18** Variation of antenna gain with frequency**Table 2** Performance comparison of the suggested antenna

S. No.	Reference	Impedance bandwidth (GHz)	Polarization	Axial ratio bandwidth (GHz)	Dimensions (mm × mm)
1	Proposed antenna	3–11	LHCP	4–9	32 × 30
2	[15]	3–11	LHCP	4–9.5	34 × 30
3	[16]	2.25–7.35	LHCP	2.05–6.55	49 × 55
4	[17]	2.4–14	LHCP	4.3–6.75	60 × 50
5	[18]	2.67–13	LHCP	4.9–6.9	60 × 60
6	[19]	4.56–8.5	RHCP	4.75–8.45	40 × 40
7	[20]	5.02–10.84	LHCP	5.07–9.22	40 × 40
8	[21]	2.08–3.75	LHCP	2.28–3.76	46.6 × 70
9	[22]	1.84–2.43	LHCP	1.89–2.43	50 × 50
10	[23]	1.48–4.24	RHCP	2.05–3.9	55 × 50
11	[24]	0.85–4.15	LHCP	1.20–3.40	100 × 100
12	[25]	1.78–5.64	RHCP	2.85–5.21	54 × 54
13	[26]	2.4–7.4	LHCP	4.9–6.9	39 × 32

be attained compared to simulated and tested results. The tested gain of the antenna varies in between 4.5 and 7 dB for complete UWB. Table 2 indicates the performance evaluation of the suggested structure with those recent antennas in the publication. It is noticed that the proposed structure has a small size with wider impedance bandwidth and ARBW than the existing antenna.

### 3 Conclusion

In this letter, a compact ring-shaped CP UWB antenna has been effectively simulated and tested. The CP UWB antenna is attained by inserting a slot in the ground that generates rotating surface current to produce CP characteristic's in this antenna. The surface current moves in the clockwise direction when observed from +Z direction and LHCP is obtained. Simulated and tested results confirm that the suggested CP UWB antenna obtains impedance bandwidth of 3–11 GHz and ARBW of 4–9 GHz as observed from +Z direction. So, suggested antenna is a decent applicant for wideband CP application like WiMAX (3.3–3.6 GHz), 5G (3.4–3.7 GHz), C-band (3.7–4.2 GHz), Aeronautical Radio Navigation band (4.2–4.7 GHz), WLAN (5.15–5.825 GHz), downlink of X-band satellite communications (7.25–7.75 GHz) and X-band satellite link (9.6–11.2 GHz) within the UWB frequency range.

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**Author Contributions** Authors have contributed a compact circular polarised ultra wide band antenna.

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### Declarations

**Conflict of interest** The authors have no conflict of interest to declare that are relevant to the content of this article.

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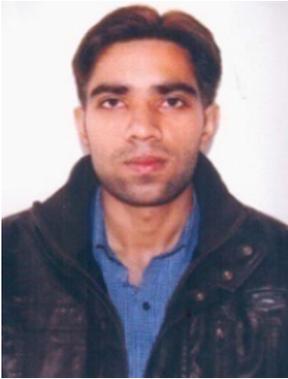
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18 months prior joining Technical Officers' branch of the I.A.F. and Advanced Stage Trade Training Wing at Guided Weapon Training Institute, Baroda He was also a recognized postgraduate teacher in microwave communication at Pune University. His research interest is in the area of conformal microstrip patch antenna for aircraft systems. His publications in referred journals and conferences are well cited. His previous assignments includes, Deputy Director at Air Headquarters and were involved in planning, coordinating and directing maintenance, modification of aircraft and helicopter systems, modifications and induction of advance electronic systems into I.A.F., Commanding Officer of an 8 GHz LOS microwave communication unit, Senior Engineer looking after maintenance of airfield navigation aids, techno-logistic management of ground based communication equipment as Aeronautical Engineering (Electronics) Branch officer of the I.A.F., Chairman Communication Advisory Committee at I.A.T. Pune. He is qualified for first & second line servicing of Mirage-2000 aircraft. Work experience on Mirage Mission Simulator and fly by wire systems of Mirage-2000 aircraft. Led and supervised highly qualified and skilled engineering officers and technicians of I.A.F. in maintenance and operation of missile, radar and communication systems. Experienced in management of resources to achieve time bound targets and objectives viz. successfully implemented contract with international and national agencies for induction of Unmanned Aerial Vehicle, Portable Laser Designating Systems and up gradation of aircraft simulators for the I.A.F. Prior to joining JUIT Waknaghat as Director and academic head, he was a Professor in the department of ECE at Jaypee Institute of Information Technology (JIIT), Noida. He also initiated training and placement process for JIIT, Noida. Successfully placed first and second batch students of Jaypee Education System in top-notch national and multinational organizations through campus recruitment. He has been associated at JIIT, Noida in students' welfare and discipline as Associate Dean of Students and Chairman Proctorial Board respectively.